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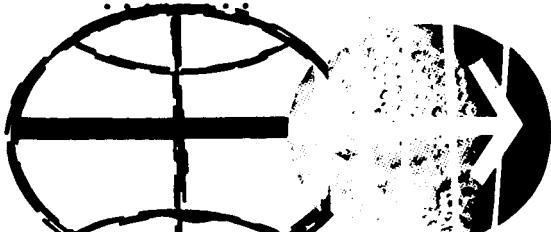
COMPARISON OF  
NAVIGATION SYSTEMS IN  
EARTH ORBIT

By Michael J. Oles, USAF

Mathematical Physics Branch



MISSION PLANNING AND ANALYSIS DIVISION



MANNED SPACECRAFT CENTER  
HOUSTON, TEXAS

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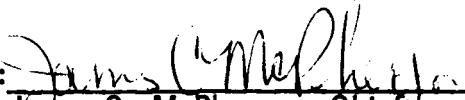
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## COMPARISON OF NAVIGATION SYSTEMS

### IN EARTH ORBIT

By Michael J. Oles, USAF

#### SUMMARY

Three procedures have been studied to determine which best utilizes the capabilities of the S-IVB instrumentation unit (S-IVB IU), command module (CM), and ground navigation systems during the earth parking orbit (EPO). The procedures are (1) using the S-IVB IU alone, (2) combining the IU and ground, and (3) combining the CM system and ground. The systems were evaluated by determining the velocity required (i.e.,  $\Delta V$  cost) for the first translunar midcourse correction (MCC) using existing error analysis programs.

The results of the study show that it is desirable, but not necessary, to update the S-IVB IU estimate of position and velocity in the EPO. If the CM navigation system is prime for navigating through the TLI maneuver, it is desirable to perform an inertial platform alignment in EPO. The S-IVB IU platform drift in EPO appears to contribute greatly to the  $\Delta V$  cost of the first MCC.

The study indicates that, for the first 10 hours after translunar insertion (TLI), the time the first MCC is performed does not significantly influence the size of the correction. The  $\Delta V$  cost does not seem to differ for various launch azimuths, lunar declinations at pericynthion, and the constraints they cause on the tracking profiles.

The  $\Delta V$  costs presented in this report should not be considered as being actual; rather, they should be considered as criteria for comparing the three navigation systems.

#### INTRODUCTION

In the earth orbit phase of the Apollo lunar landing mission there are three navigation systems operating - the S-IVB IU, the CM guidance and navigation equipment, and the ground tracking complex. For convenience, the S-IVB navigation system, hardware, and software will be referred to as the IU in this report. To determine the navigation procedure which best utilizes these capabilities, estimates of the uncertainty in position and velocity were computed and evaluated in terms of the first midcourse correction for three navigation procedures - IU

alone, IU and ground, and CM and ground. In studying the procedures the following areas were investigated:

1. Whether to update the IU estimate of position and velocity with the ground estimate.
2. The use of CM instead of IU navigation to execute the TLI maneuver.
3. The effects of platform misalignment and other hardware errors on the first MCC  $\Delta V$  cost.
4. How the time of the first MCC affects  $\Delta V$  cost.
5. The influence of launch azimuth and lunar declination at pericynthion on the first MCC  $\Delta V$  cost.

#### The S-IVB IU Navigation System

The IU contains a navigation system which can maintain an estimate of position and velocity ( $R$  and  $V$ ) throughout the launch phase, earth parking orbit (EPO) phase, and TLI maneuver. During the EPO phase, the IU integrator includes the effects of an atmospheric model, a venting model, and four zonal harmonics, but no accelerometer readings.

During the launch phase and the TLI maneuver, the IU accelerometers, which are attached to an inertially oriented platform, measure vehicle accelerations due to thrust. These acceleration measurements are passed to a predictor which integrates thrust acceleration as well as the gravitational accelerations (including the effects of two zonal harmonics) to obtain  $R$  and  $V$ .

A ground-computed  $R$  and  $V$  may be transmitted during EPO to replace the IU-computed  $R$  and  $V$ . Replacement of the onboard-computed vector by a ground-computed vector is called an update.

Although it may drift from its inertial orientation, the inertial platform within the IU cannot be realigned after the launch phase has begun.

#### The CM Navigation System

The CM contains a navigation system which is capable of maintaining an estimate of  $R$  and  $V$  during the entire lunar landing mission. Because its free-flight integrator does not consider atmospheric or venting accelerations, the CM estimate of position and velocity during EPO will be updated prior to TLI. During EPO, the CM inertial platform may be realigned. The thrust accelerations during powered flight are measured

by accelerometers attached to an inertial platform within the CM. These readouts are passed to its predictor which integrates the gravitational and thrust accelerations.

#### Ground Navigation System

The ground navigation system can determine an estimate of the vehicle's position and velocity during all mission phases. The following sources of information can be used to obtain this estimate:

1. A global network which includes unified S-band (USBS) and C-band tracking facilities.
2. IU- or CM-computed R and V vectors telemetered to the Real-Time Computer Complex (RTCC).
3. Vehicle vectors computed by RTCC free- and powered-flight integrators.

The information obtained from these three sources can be combined at the RTCC to obtain a ground-estimated vector.

During EPO, the RTCC free-flight Encke integrator includes a gravitational model with one tesseral and three zonal harmonics, the perturbative effects of the sun and moon, and venting and atmospheric models. At insertion into earth parking orbit, the IU estimate of R and V may be used by the ground navigation system as its initial estimate. After the TLI maneuver the ground navigation system determines the position and velocity of the vehicle.

#### ANALYSIS

The three navigation systems were compared in the following manner.

The statistical deviation of the estimated from the actual R and V(covariance matrix) at the start of TLI was computed for the three procedures using various launch azimuths and injection opportunitites (appendix A). These deviations were then propagated through the TLI maneuver considering, as applicable, either IU or CM navigation errors during the maneuver (appendix B). The covariance matrix at the end of TLI represents the deviation of the IU or CM estimate from the actual R and V. This study assumes that if this deviation were zero, the vehicle would pass through the desired TLI target position near the moon; i.e., the estimated and desired R and V were assumed equal at TLI cutoff. The covariance matrices at TLI cutoff, considered to represent deviations of the actual from the desired R and V, were then propagated to the time of the first MCC. The  $\Delta V$  cost of the correction

was computed as a function of the covariance matrix at the time of the first MCC (appendix C).

## RESULTS

Table I concisely presents first MCC  $\Delta V$  costs for each of the three combinations of navigation systems. The first MCC was assumed to occur either 5 or 10 hours after TLI. The following discussion refers to the first MCC when made 5 hours after TLI. A comparison of the IU alone against the ground and IU navigation systems combined is presented for a  $72.6^\circ$  launch azimuth and  $-27.5^\circ$  lunar declination in table I. These conditions offer a TLI opportunity at 86.0 minutes after EPO insertion (EPOI). If a vector update of the IU occurs 50 minutes after EPOI (see appendix A for the various tracking profiles), the  $\Delta V$  cost of the first MCC is 3.35 fps. If the same conditions exist and no update is made, the  $\Delta V$  cost of the first MCC is 4.93 fps.

A second TLI opportunity having a  $72.6^\circ$  launch azimuth and  $-27.5^\circ$  lunar declination occurs 260.5 minutes after EPOI; this is probably the longest time expected for the earth parking orbit phase. If an update of the IU estimate is made 228 minutes after EPOI with this TLI opportunity, the midcourse  $\Delta V$  cost is 8.62 fps. When no update of the IU is made, the  $\Delta V$  cost of the first MCC is 12.75 fps.

When the TLI opportunity is close to the time of insertion (86 minutes), the difference between the first MCC  $\Delta V$  cost using both the ground and IU and using the IU navigation alone is about 1.5 fps. When the TLI opportunity is far from insertion (260.5 minutes), the difference is about 4.1 fps.

If the IU inertial platform is considered to drift in the EPO and if the IU is updated 50 minutes in the EPO with an injection opportunity 86.0 minutes in the EPO, the  $\Delta V$  cost is 3.35 fps. It would be 2.09 fps if the platform did not drift in EPO. The  $\Delta V$  cost due to platform drift is therefore 1.26 fps.

If the IU is not updated and the TLI opportunity occurs at 260.5 minutes after EPOI, the  $\Delta V$  cost due to platform drift in earth orbit is 2.77 fps.

A comparison of all three navigation system combinations (IU alone, IU and ground, CM and ground) is also presented in table I. Based on a  $90^\circ$  launch azimuth and a  $-27.5^\circ$  lunar declination, a TLI opportunity occurs 176.0 minutes after EPOI. If a vector update of the IU occurs 135 minutes after EPOI, the  $\Delta V$  cost for first MCC is 5.88 fps; with no update, the  $\Delta V$  cost is 8.24 fps. If the CM vector is updated, the  $\Delta V$  cost is 12.6 fps if the CM platform is not realigned in EPO and 8.51 fps if it is realigned.

Table II presents the results in more detail. The table presents the difference between IU and ground combined and the IU alone and the difference between the IU and ground combined and the CM and ground combined. Table III details the  $\Delta V$  cost at the first MCC as a function of individual error sources. The results in table II and table III are graphed in figures 1 through 4.

#### CONCLUSIONS

From the results of this study (tables I and II and fig. 1 through 4), the following conclusions are drawn.

1. In view of the small  $\Delta V$  saving which occurs when the S-IVB IU estimate of position and velocity is updated in EPO, it appears to be desirable, but not necessary, to perform the update.
2. From figure 3 it appears that, up until two revolutions in the EPO phase, the IU performs the TLI maneuver with no update better than the CM can with a platform alignment in EPO and a ground-computed vector update used as the spacecraft's position and velocity vector at the start of TLI. When a ground update of the CM vector has been made as explained in the appendices, but no platform alignment is effected, the  $\Delta V$  cost of the first MCC always appears to be worse than if the S-IVB IU navigated through the maneuver but had no ground update in EPO.
3. IU platform misalignment appears to be the major contributor to the  $\Delta V$  cost as portrayed in figures 1 through 3. Figure 3 indicates that it is quite desirable to align the CM inertial platform in EPO.
4. This study indicates that the time the first MCC is performed does not significantly influence the size of the corrections for the first 10 hours after TLI.
5. The  $\Delta V$  cost of the first MCC did not seem to differ significantly for various launch azimuths, lunar declinations, and the constraints they cause on the tracking profiles, when similar times of TLI opportunities were compared.

TABLE I.- A SUMMARY OF THE ΔV COST OF THE FIRST MCC

## (a) TU and ground

Launch azimuth, deg	Lunar declination, deg	Time of TLI in minutes after EPOI	Approximate time of vector update, (if applicable), in minutes after EPOI (a)	Navigation systems considered	ΔV cost of the 1st MCC		
					1st MCC 5 hours after TLI	1st MCC 10 hours after TLI	IU platform drift in EPO considered
72.6	-27.5	86.0	--	IU TU and ground	4.93	5.66	4.17
72.6	-27.5	86.0	50.	IU TU and ground	3.35	3.47	2.09
72.6	-27.5	260.5	--	IU TU and ground	12.75	13.35	9.98
72.6	-27.5	260.5	228.	IU TU and ground	8.62	8.75	3.35
90.0	-27.5	176.0	--	IU TU and ground	8.24	8.83	6.26
90.0	-27.5	176.0	135.	IU TU and ground	5.88	5.94	2.39

## (b) CM

Launch azimuth, deg	Lunar declination, deg	Time of TLI in minutes after EPOI	Approximate time of vector update in minutes after EPOI	Navigation systems considered	ΔV cost of the 1st MCC		
					CM inertial platform realigned approximately 1/2 hour prior to TLI	CM inertial platform realigned approximately 1/2 hour prior to TLI	No CM inertial platform alignment during EPO
90.0	-27.5	176.0	b <sub>135</sub> .	CM and ground	8.51	11.0	12.6
90.0	-27.5	176.0	b <sub>135</sub> .	CM and ground	8.51	11.0	14.4

<sup>a</sup>See Appendix A for ground track profile.<sup>b</sup>The update was uplinked to the CM at this time, but the values were those predicted by the ground navigation system to the start of TLI.

TABLE III.-  $\Delta V$  COST OF THE FIRST MCC

Launch azimuth, deg	Lunar declination, deg	Time of TLI in minutes after EPOI	Approximate time of vector update (if applicable) in minutes after EPOI (a)	Navigation systems considered	$\Delta V$ cost of the 1st MCC			
					IU platform drift in EPO considered		No IU platform drift in EPO considered	
					1st MCC 5 hours after TLI	1st MCC 10 hours after TLI	1st MCC 5 hours after TLI	1st MCC 10 hours after TLI
(a) IU and Ground								
72.6	+27.5	131.0	--	IU	5.28	5.45	3.45	3.78
72.6	+27.5	145.0	--		5.90	6.12	3.92	4.30
72.6	+27.5	218.5	--		9.45	9.67	6.70	7.11
72.6	+27.5	232.5	--		10.17	10.42	7.29	7.74
72.6	+27.5	131.0	90.	IU and Ground	4.34	4.33	1.68	1.80
72.6	+27.5	145.0	90.		4.89	4.94	2.10	2.33
72.6	+27.5	218.5	180.		6.87	6.79	1.67	1.75
72.6	+27.5	232.5	180.		7.28	7.20	1.69	1.75
72.6	-27.5	86.0	--	IU	4.93	5.66	4.17	5.03
72.6	-27.5	101.0	--		5.60	6.32	4.68	5.54
72.6	-27.5	173.0	--		8.27	8.89	6.37	7.21
72.6	-27.5	188.5	--		9.19	9.82	7.17	8.03
72.6	-27.5	260.5	--		12.75	13.35	9.98	10.82
72.6	-27.5	86.0	50.	IU and Ground	3.35	3.47	2.09	2.31
72.6	-27.5	101.0	50.		4.41	4.76	3.15	3.67
72.6	-27.5	173.0	136.		6.10	6.26	3.06	3.49
72.6	-27.5	188.5	136.		6.23	6.60	3.10	3.41
72.6	-27.5	260.5	228.		8.62	8.75	3.35	3.91
90.0	-27.5	168.0	--	IU	7.19	7.92	5.46	6.10
90.0	-27.5	176.0	--		8.24	8.83	6.26	7.08
90.0	-27.5	256.0	--		11.99	12.45	9.09	9.79
90.0	-27.5	168.0	135.	IU and Ground	5.56	5.60	2.16	2.42
90.0	-27.5	176.0	135.		5.88	5.94	2.39	2.70
90.0	-27.5	256.0	197.		8.34	8.37	2.95	3.31

<sup>a</sup>See Appendix A for ground track profile.

TABLE II.-  $\Delta V$  COST OF THE FIRST MCC - Concluded

## (a) IU and Ground - Concluded

Launch azimuth, deg	Lunar declination, deg	Time of TLI in minutes after EPOI	Approximate time of vector update (if applicable) in minutes after EPOI (a)	Navigation systems considered	$\Delta V$ cost of the 1st MCC	
					1st MCC 5 hours after TLI	1st MCC 5 hours after TLI
108.0	-27.5	85.0	--	IU	4.80	5.50
108.0	-27.5	157.5	--		6.67	6.91
108.0	-27.5	172.5	--		8.20	8.79
108.0	-27.5	244.5	--		11.05	11.35
108.0	-27.5	85.0	55.	IU and Ground	3.14	3.20
108.0	-27.5	157.5	83.		5.56	5.68
108.0	-27.5	172.5	147.		6.00	6.08
108.0	-27.5	244.5	172.		9.22	9.49

## (b) CM and Ground

Launch azimuth, deg	Lunar declination, deg	Time of TLI in minutes after EPOI	Approximate time of vector update in minutes after EPOI.	Navigation systems considered	$\Delta V$ cost of the 1st MCC	
					CM inertial platform realigned approximately 1/2 hour prior to TLI	No CM inertial platform alignment during EPO
90.0	-27.5	168.0	b135.	CM and Ground	8.44	10.9
90.0	-27.5	176.0	b135.		8.51	11.0
90.0	-27.5	256.0	b197.		8.68	11.2

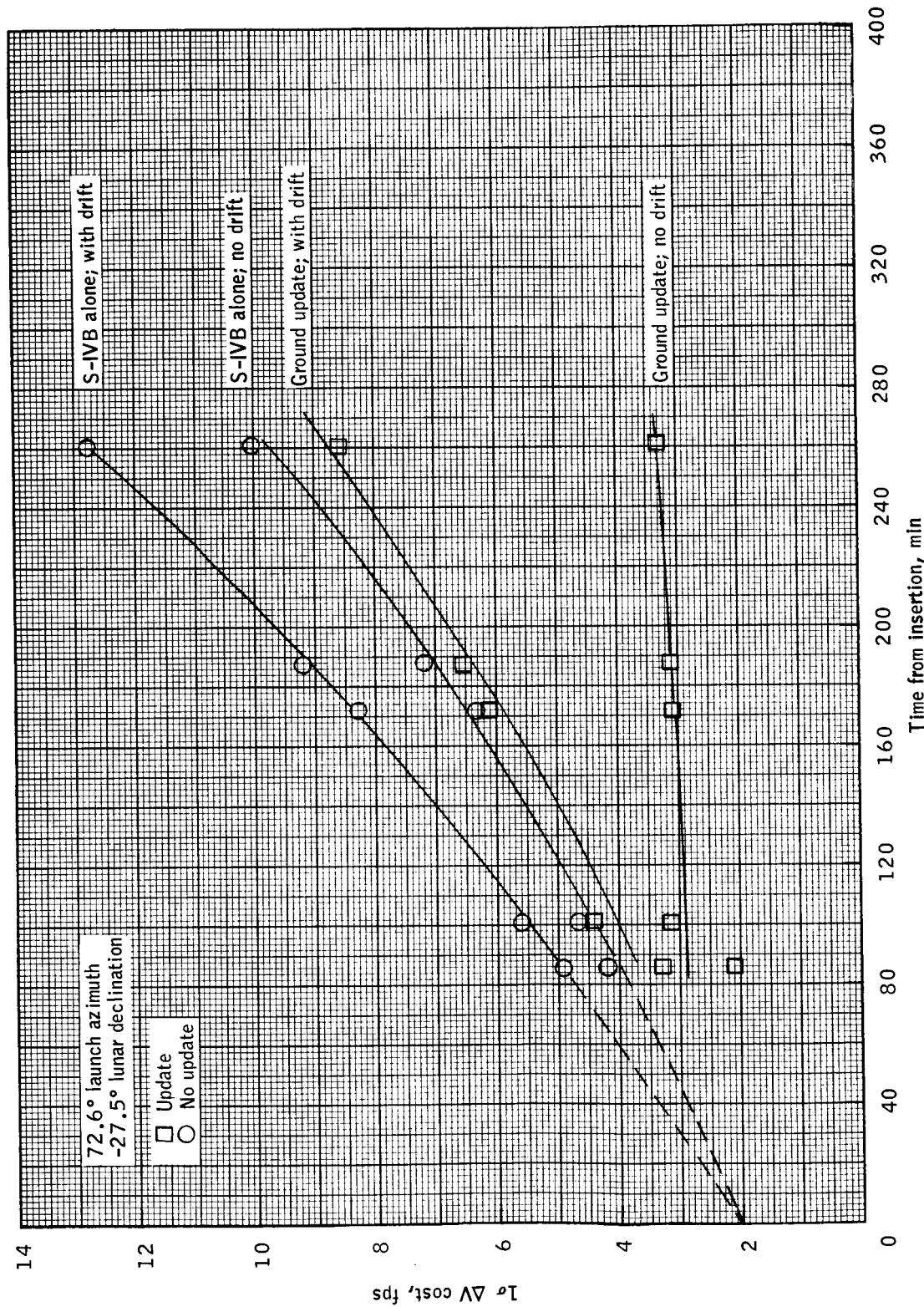
<sup>a</sup>See Appendix A for ground track profile.<sup>b</sup>The update was uplinked to the CM at this time, but the values were those predicted by the ground navigation system to the start of TLI.

TABLE III.- EFFECT OF INDIVIDUAL ERROR SOURCES ON THE FIRST MCC

Time of TLI, minutes after EPOI	Approximate time of vector update (if applicable), minutes after EPOI	Individual error sources of the ground and IU.	$\Delta V$ cost of the 1 <sup>st</sup> MCC	
			1 <sup>st</sup> MCC 5 hours after TLI	1 <sup>st</sup> MCC 10 hours after TLI
Anytime	Anytime <sup>a</sup>	IU scale factor and bias during TLI. Other IU navigation hardware and software perfect.	0.45	0.60
Launch azimuth and lunar declination not applicable				
86.0	<sup>a</sup> 86.0	IU launch pad misalign- ment and drift to TLI.	2.92	2.88
101.0	<sup>a</sup> 101.0	Other IU navigation hard- ware and software perfect	3.34	3.29
173.0	<sup>a</sup> 173.0		5.43	5.35
188.5	<sup>a</sup> 188.5		5.89	5.80
260.5	<sup>a</sup> 260.5		8.04	7.92
72.6° Launch azimuth; -27.5° lunar declination				
86.0	--	IU estimate of position and velocity at the start of TLI in error due to IU navigation errors during the launch and earth orbit phases. Perfect IU navigation during the TLI maneuver.	3.94	4.84
101.0	--		4.48	5.36
173.0	--		6.23	7.07
188.5	--		7.04	7.90
260.5	--		9.88	10.7
72.6° Launch azimuth; -27.5° lunar declination				
86.0	<sup>b</sup> 50.0	IU estimate of position and velocity at the start of TLI in error due to ground navigation error and IU earth orbit navigation error from the time of the update to the start of TLI. Perfect IU navigation during the TLI maneuver.	1.58	1.84
101.0	<sup>b</sup> 50.0		2.84	3.38
173.0	<sup>b</sup> 136.0		2.74	3.19
188.5	<sup>b</sup> 136.0		2.78	3.09
260.5	<sup>b</sup> 228.0		3.07	3.67

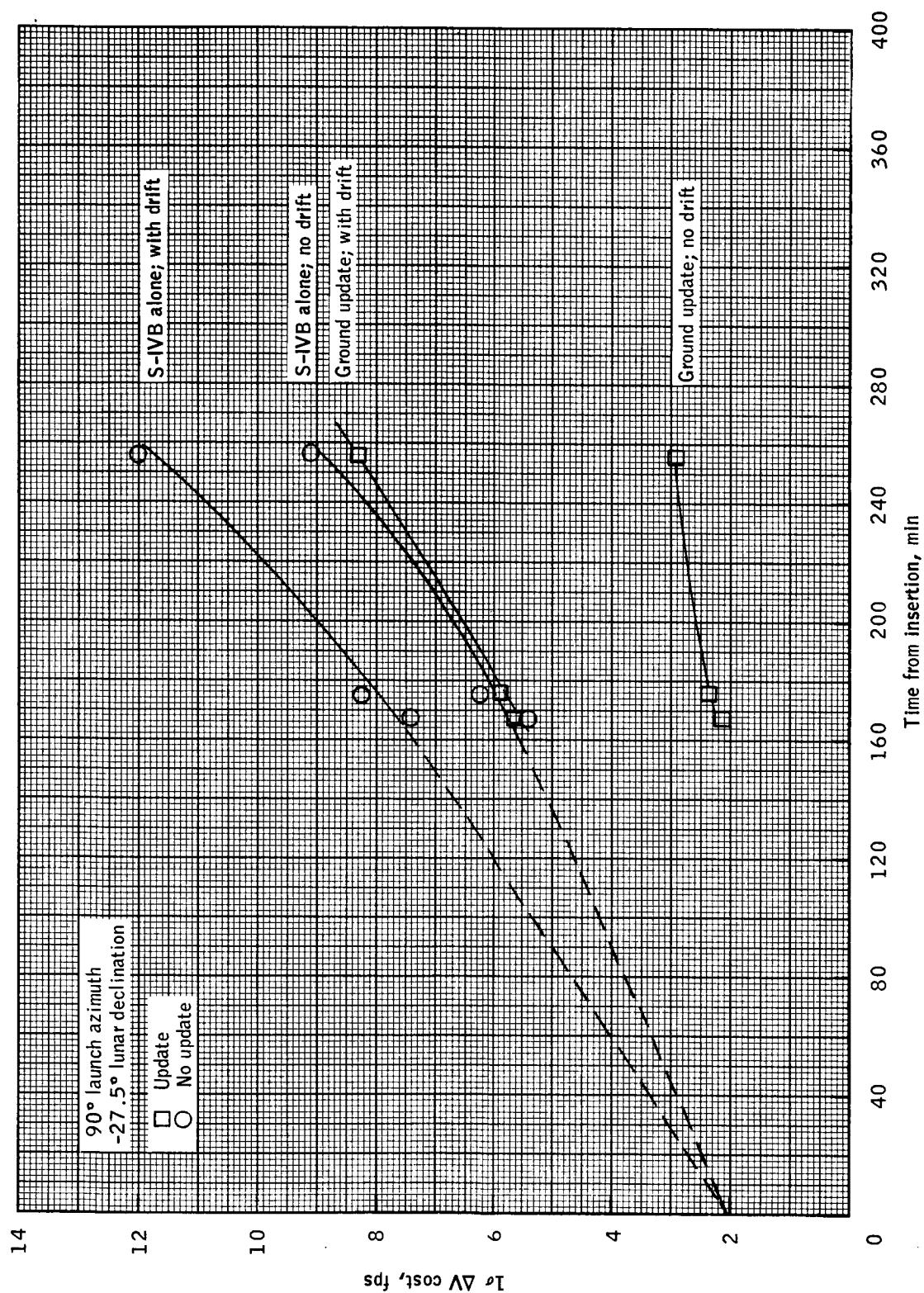
<sup>a</sup>Perfect update uplinked to IU.

<sup>b</sup>See Appendix A for ground track profile.



(a) 72.6° launch azimuth; -27.5° lunar declination.

Figure 1.-  $\Delta V$  cost with and without ground update and platform drift for a midcourse correction 5 hours from translunar injection.



(b) 90° launch azimuth; -27.5° lunar declination.

Figure 1.- Continued.

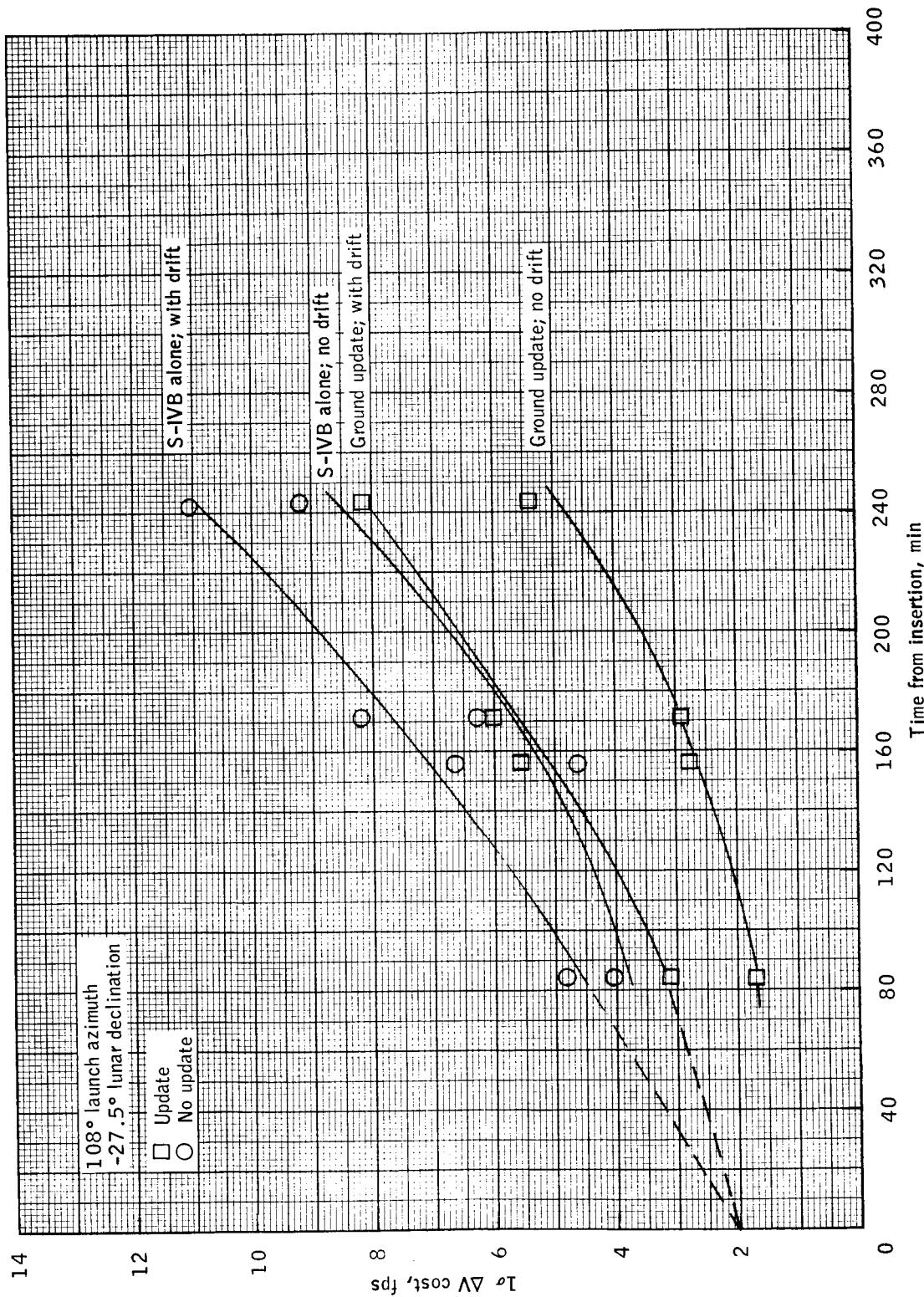
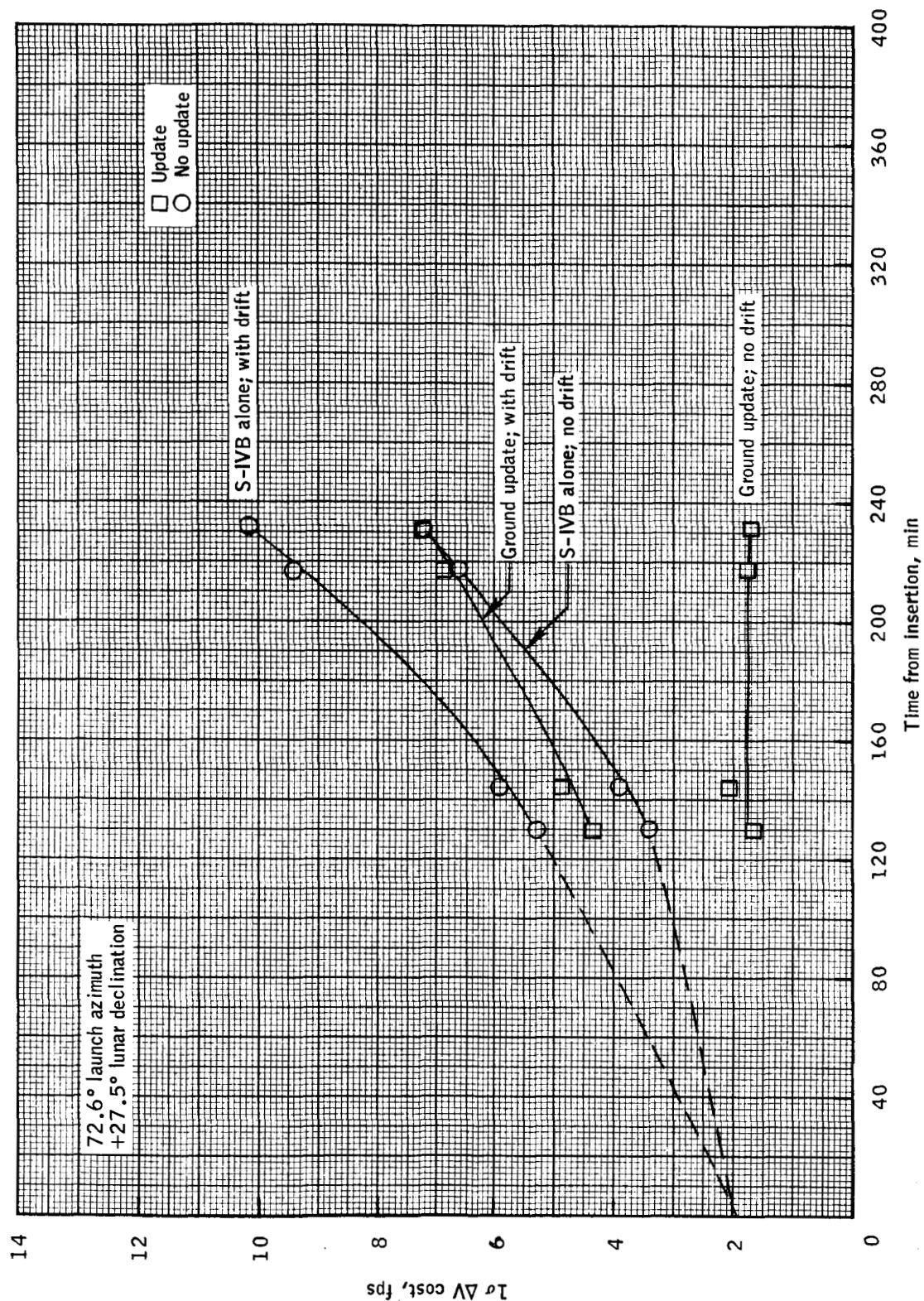
(c)  $108^\circ$  launch azimuth;  $-27.5^\circ$  lunar declination.

Figure 1.- Continued.



(d) 72.6° launch azimuth; +27.5° lunar declination.

Figure 1.- Concluded.

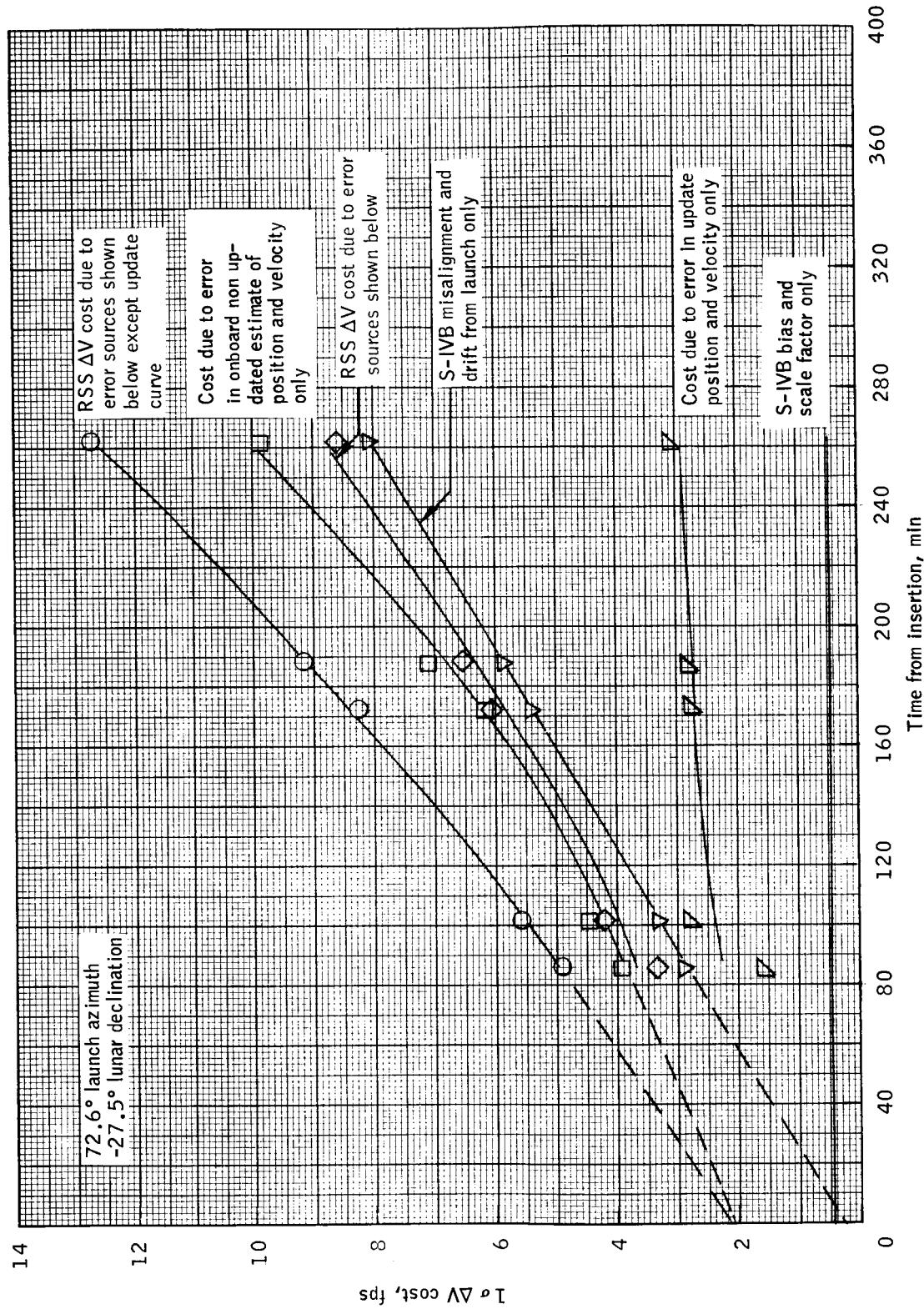


Figure 2.-  $\Delta V$  cost due to individual error sources for a midcourse correction five hours from translunar injection.

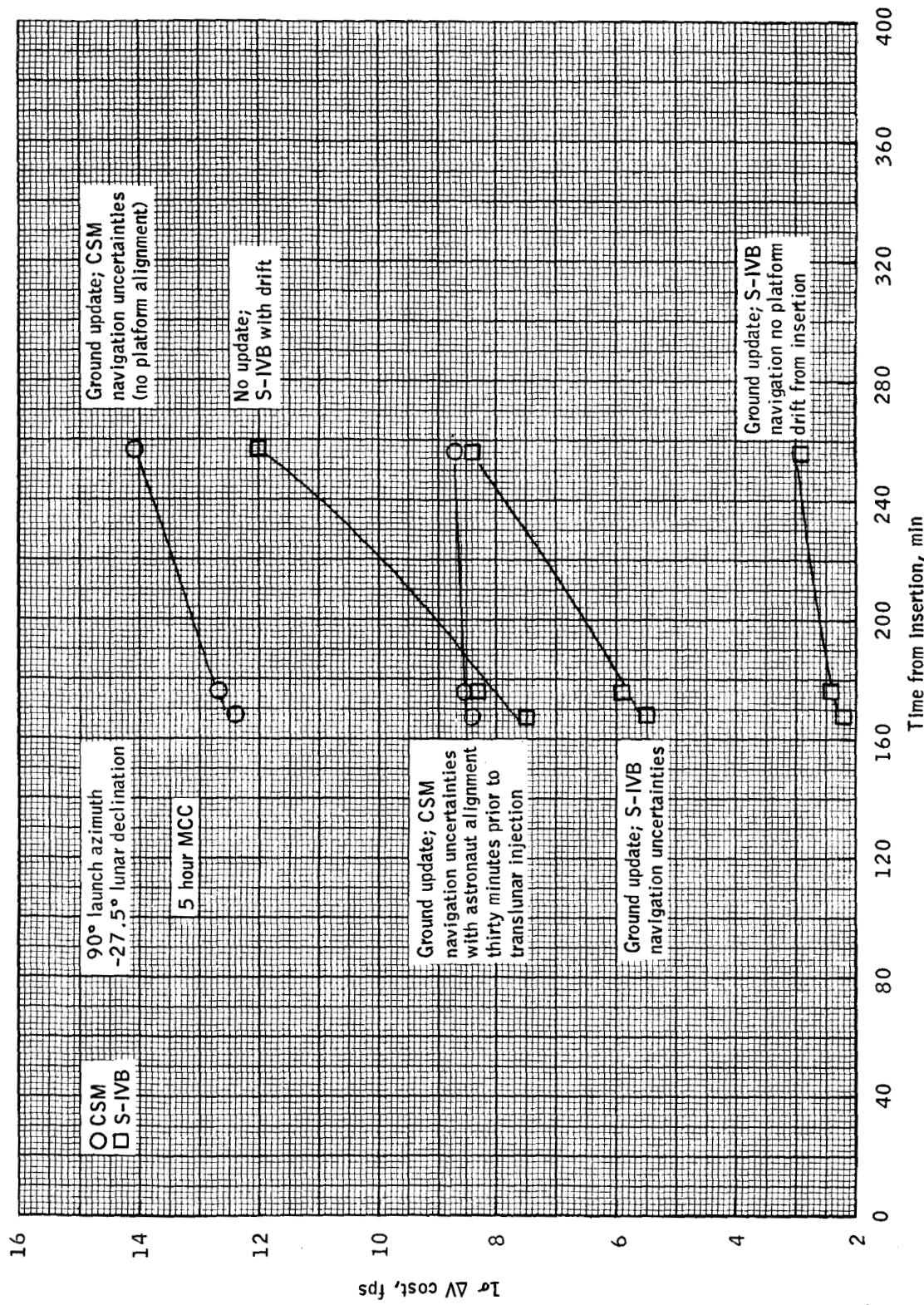


Figure 3. - Comparison of S-IVB and spacecraft maneuver navigation.

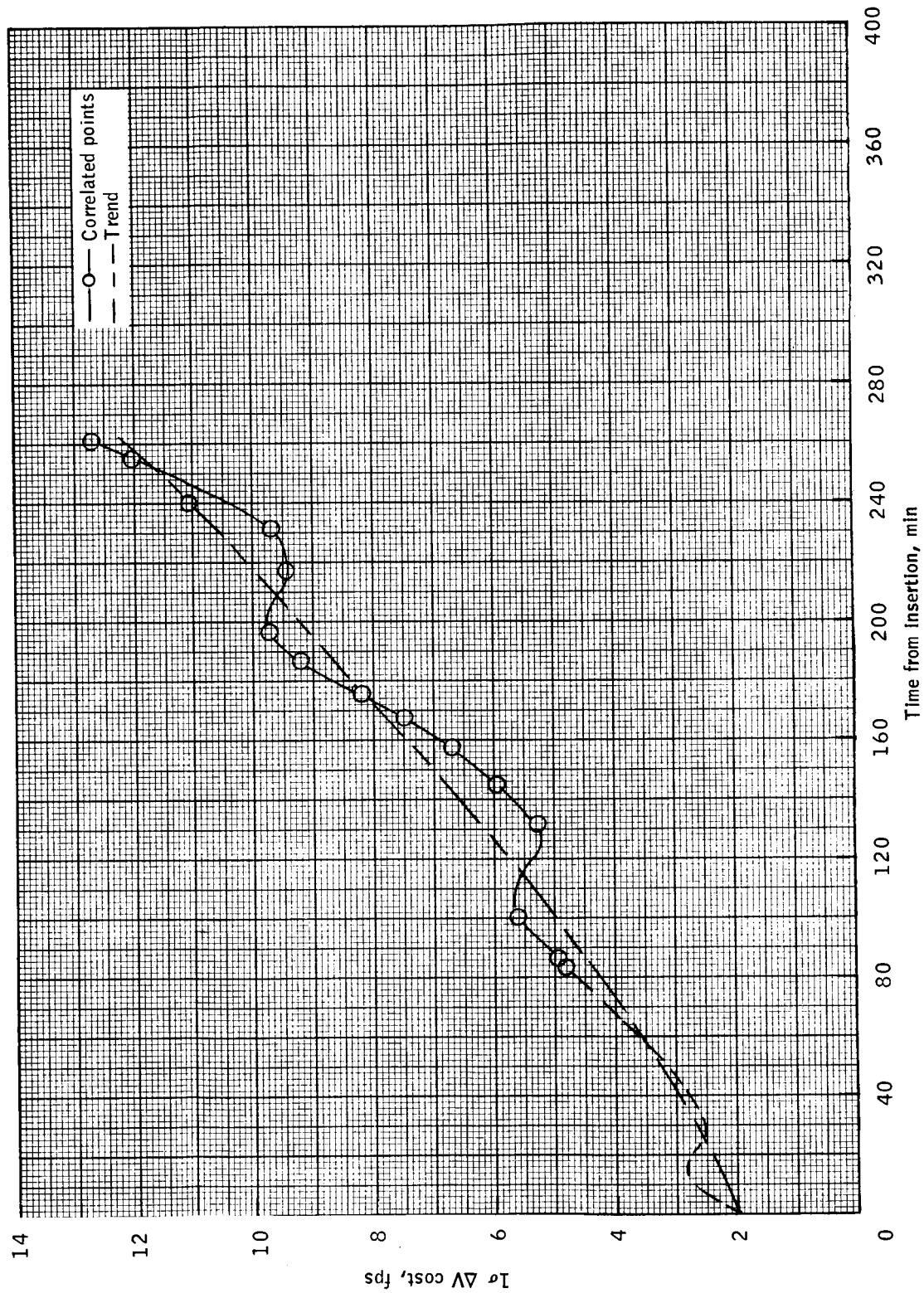


Figure 4.-  $\Delta V$  cost based on S-IVB navigation, no update, and a midcourse correction five hours from translunar injection.

APPENDIX A  
EARTH PARKING ORBIT PROCEDURES

## APPENDIX A

## EARTH PARKING ORBIT PROCEDURES

This appendix presents the procedures used in the EPO to generate covariance matrices expressing deviations of the onboard estimate of position and velocity from the actual position and velocity at the start of the TLI maneuver.

The matrices were computed under a separate task (ref. 1), using the Bissett-Berman Orbit Error Analysis Program (BBOEAP). A detailed discussion on the program is found in reference 2.

The TLI injection opportunities depend on the launch azimuth, lunar declination at pericynthion, and constraints in the updating procedures. The injection points are given in table A-I.

Table A-I was obtained by determining the latitude and longitude of the vehicle at TLI and the time of TLI with the Bissett-Berman Visibility and Ground Track Program (BBVGTP) - (ref. 3).

The BBVGTP was also used to determine the C- and S-band stations capable of observing the vehicle for various earth parking orbit insertion conditions. Table A-II was formed considering only C-band tracking in EPO with the possibility of a C-band or S-band station updating the onboard vector. It includes the preliminary mission constraint that the update, if it occurs, must be made 30-90 minutes prior to TLI. Observations of range and azimuth and elevation angles taken by the C-band stations occurred at 6-second intervals.

The covariance matrices expressing the deviation of the estimated from the actual values were propagated in EPO to the start of TLI. This study assumes the ground navigation system has no knowledge of the vehicle's position and velocity at insertion into earth parking orbit. During periods of no tracking, the covariance matrices of the ground-computed estimates were propagated considering errors in the venting, gravitational, and drag accelerations. During tracking intervals, errors in the observables were considered in the covariance matrices. Table A-III includes the ground track error model assumed for the ground navigation system.

If the IU estimate is updated in earth orbit, its estimate at the start of TLI deviates from the actual because of the error in the update and error in the IU prediction model after the time of the update. If

the IU estimate is not updated in earth orbit, the error at the start of TLI is due to the error in the IU earth orbit insertion conditions and the error in the IU prediction model in earth orbit. This study assumed the ground and IU navigation systems had the same free-flight prediction model. The errors in both, during free flight and periods of no tracking were modeled as gravitational, venting, and drag acceleration uncertainties shown in the footnote to table III.

The error in the IU estimate of position and velocity at insertion into an earth parking orbit was obtained in the following manner:

Reference 4 describes the deviation of the actual from the IU estimate of the position and velocity of the vehicle at insertion due to  $3\sigma$  navigation errors. The dispersions are  $3\sigma$  based on  $3\sigma$  perturbations of the navigation parameters. Although the covariance of the onboard uncertainty was not explicitly given at insertion, it was built in the following manner. Let

$$\frac{1}{3} \begin{bmatrix} \frac{3\Delta x_1}{\sigma_{P_1}} & \frac{3\Delta x_2}{\sigma_{P_2}} & \frac{3\Delta x_3}{\sigma_{P_3}} & \dots & \frac{3\Delta x_{30}}{\sigma_{P_{30}}} \\ \frac{3\Delta y_1}{\sigma_{P_1}} & \frac{3\Delta y_2}{\sigma_{P_2}} & \frac{3\Delta y_3}{\sigma_{P_3}} & \dots & \frac{3\Delta y_{30}}{\sigma_{P_{30}}} \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ \frac{3\Delta z_1}{\sigma_{P_1}} & \frac{3\Delta z_2}{\sigma_{P_2}} & \frac{3\Delta z_3}{\sigma_{P_3}} & \dots & \frac{3\Delta z_{30}}{\sigma_{P_{30}}} \end{bmatrix} = \Omega$$

$6 \times 30$

and  $P = \text{diagonal } (\sigma_{P_1}^2, \sigma_{P_2}^2, \sigma_{P_3}^2, \dots, \sigma_{P_{30}}^2) 30 \times 30$

where  $(3 \Delta S_i)$ ,  $i = 1, 30$ ;  $S = x, y, z, \dot{x}, \dot{y}, \dot{z}$  are the  $3\sigma$  dispersions of the state at insertion and  $\sigma_{P_i}$ ,  $i = 1, 30$  corresponding to the navigation uncertainties.

Then  $\Omega_{6 \times 30}^T P_{30 \times 30} \Omega_{30 \times 6} = (\text{covariance of state at insertion})_{6 \times 6}$   
 obtained by  

$$\sigma_{ij}^2 = \frac{1}{9} \sum_{k=1}^{30} (3\Delta i_k) (3\Delta j_k) \quad i, j = x, y, z, \dot{x}, \dot{y}, \dot{z}$$

where  $k$  is the navigation parameter causing the particular dispersion.  
 Thus,

$$\begin{aligned} \sigma_{xx}^2 &= \frac{1}{9} (3\Delta x_1) (3\Delta x_1) + \frac{1}{9} (3\Delta x_2) (3\Delta x_2) + \\ &\dots + \frac{1}{9} (3\Delta x_{30}) (3\Delta x_{30}) \end{aligned}$$

and

$$\begin{aligned} \sigma_{yz}^2 &= \frac{1}{9} (3\Delta y_1) (3\Delta z_1) + \frac{1}{9} (3\Delta y_2) (3\Delta z_2) + \\ &\dots + \frac{1}{9} (3\Delta y_{30}) (3\Delta z_{30}) \end{aligned}$$

etc.

The covariance matrix obtained at insertion was expressed in a plumbline system defined at lift-off as follows:

The Y-axis parallel to and positive to the vehicle radius vector at lift-off.

The X-axis in the plane of the vehicle's motion, positive down-range, perpendicular to y.

The Z-axis completes a right-handed orthogonal system.

It was rotated to the local vertical system to be used in the BBOEAP. The local vertical system is defined as follows:

The X-axis parallel to and positive in the direction of the vehicle radius vector at the time of interest.

The Y-axis is in the plane of the vehicle's motion positive down-range, perpendicular to X.

The Z-axis forms the right-handed orthogonal system.

The rotation was accomplished in two steps. The first was to rotate the matrix into the local vertical system defined at lift-off.

Denoting the local vertical system by primes,

$$\begin{bmatrix} \Delta x \\ \Delta y' \\ \Delta z' \\ \vdots \\ \Delta x' \\ \vdots \\ \Delta y' \\ \vdots \\ \Delta z' \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & & \\ 1 & 0 & 0 & & \\ 0 & 0 & -1 & & \\ & & & \bar{0} & \\ & & & & 0 & 1 & 0 \\ & & & & \bar{0} & 1 & 0 \\ & & & & 0 & 0 & -1 \end{bmatrix} \begin{bmatrix} \Delta x \\ \Delta y \\ \Delta z \\ \Delta x' \\ \vdots \\ \Delta y' \\ \vdots \\ \Delta z' \end{bmatrix} = R \begin{bmatrix} \Delta x \\ \Delta y \\ \Delta z \\ \Delta x' \\ \vdots \\ \Delta y' \\ \vdots \\ \Delta z' \end{bmatrix}$$

where  $\bar{0}$  denotes the null matrix.

Taking the expectation of both sides,  $P' = R P R^T$ , where  $P$  is the covariance of the state in the plumbline system and  $P'$  is the covariance of the state in the local vertical at time of launch.  $P'$  was then rotated through the central angle between the launch pad and insertion vector by an in-plane rotation about the  $z'$  axis. This central angle is dependent on the launch azimuth (see ref. 3).

Launch azimuth, deg	Central angle, deg
72.6	27.848
90.	25.546
108.	27.654

Table A-IV presents the covariance matrices associated with these three launch azimuths at EPOI.

All of the covariance matrices presented in this report are in units of feet and feet per second expressed in a local vertical system defined at the time of interest.

The form of the covariance matrices is

$$\left( \begin{array}{cccccc} \sigma_{xx} & \sigma_{xy} & \dots & \dots & \dots & \dots \\ \cdot & \sigma_{yy} & \dots & \dots & \dots & \dots \\ \cdot & \cdot & \sigma_{zz} & \dots & \dots & \dots \\ \cdot & \cdot & \cdot & & & \end{array} \right)$$

The covariance matrices at EPOI (table A-IV) express the deviation of the S-IVB estimate from the actual in the local vertical system defined at EPOI for the three launch azimuths.

Table A-V presents the format of the covariance matrices at the start of TLI (table A-VI) considering update or no update of the IU estimate in earth orbit.

TABLE A-I.- TLI OPPORTUNITIES

Launch azimuth, deg	Lunar declination, deg	Injection opportunities, minutes after EPOI
72.6	+27.5	131. 145. 218.5 232.5
72.6	-27.5	86. 101. 173. 188.5 260.5
90.	-27.5	168. 176. 256.
108.	-27.5	85. 157.5 172.5 244.5

TABLE A-II.-- TRACKING VISIBILITY PROFILE

Injection opportunity	Station	Tracking interval, minutes past earth parking orbit insertion	Injection, minutes past earth parking orbit insertion
(a) -27.5° Lunar declination, 72.6° launch azimuth			
1st Atlantic injection <sup>a</sup>	---	---	---
1st Pacific injection	CYI CRO <sup>b,c</sup> CNB	6.5 - 10.6 42.3 - 44.1 49.1 - 52.7	86.0
2nd Atlantic injection	Same as for 1st Pacific injection	Same as for 1st Pacific injection	101.0
2nd Pacific injection (same tracking as for 1st Pacific injection plus the adjacent)	WHS EGL CNV BDA CYI <sup>b</sup> CRO <sup>b</sup>	80.1 - 82.2 82.9 - 87.1 84.3 - 88.2 88.3 - 91.9 98.9 - 102.4 135.6 - 136.2	173.0
3rd Atlantic injection	Same as for 2nd Pacific injection	Same as for 2nd Pacific injection	188.5
3rd Pacific injection (same tracking as for 2nd Pacific injection plus the adjacent)	CAL WHS EGL CNV BDA PRE CRO <sup>b,c</sup>	169.2 - 171.5 171.1 - 175.2 175.3 - 179.3 177.0 - 180.4 180.0 - 184.1 207.8 - 210.4 226.5 - 230.1	260.5

<sup>a</sup>Injection opportunity does not meet the 30 - 90 minute update criteria.

<sup>b</sup>Update occurred over the station.

<sup>c</sup>No C-band tracking.

TABLE A-II.- TRACKING VISIBILITY PROFILE - Continued

Injection opportunity	Station	Tracking interval, minutes past earth parking orbit insertion	Injection, minutes past earth parking orbit insertion
(b) $-27.5^{\circ}$ Lunar declination, $90^{\circ}$ launch azimuth			
1st Atlantic injection <sup>a</sup>	---	---	---
1st Pacific injection <sup>a</sup>	---	---	---
2nd Atlantic injection <sup>a</sup>	---	---	---
2nd Pacific injection	CRO HAW CAL WHS EGL CNV ANT ASC PRE <sup>b</sup> CRO <sup>b</sup>	41.5 - 45.7 66.9 - 69.7 76.6 - 78.6 78.7 - 82.5 83.0 - 86.9 84.3 - 88.4 89.6 - 93.3 103.4 - 106.8 114.5 - 118.5 134.3 - 137.4	168.0
3rd Atlantic injection	Same as for 2nd Pacific injection	Same as for 2nd Pacific injection	176.0
3rd Pacific injection (same tracking as for 2nd Pacific injection plus the adjacent)	HAW CAL WHS EGL CNV GBI GTI ANT ASC <sup>b</sup>	158.5 - 162.7 168.3 - 171.1 171.2 - 174.4 176.3 - 177.8 177.8 - 179.2 178.0 - 180.4 179.5 - 183.0 182.1 - 185.5 196.0 - 198.9	256.0

<sup>a</sup>Injection opportunity does not meet the 30 - 90 minute update criteria.

<sup>b</sup>Update occurred over the station.

TABLE A-II.- TRACKING VISIBILITY PROFILE - Continued

Injection opportunity	Station	Tracking interval, minutes past earth parking orbit insertion	Injection, minutes past earth parking orbit insertion
(c) +27.5° Lunar declination, 72.6° launch azimuth			
1st Atlantic injection <sup>a</sup>	---	---	---
1st Pacific injection <sup>a</sup>	---	---	---
2nd Atlantic injection	CYI CRO WHS EGL CNV BDA <sup>b</sup>	6.5 - 10.6 42.3 - 44.1 80.1 - 82.2 82.9 - 87.1 84.3 - 88.2 87.8 - 91.9	131.0
2nd Pacific injection	Same as for 2nd Atlantic injection	Same as for 2nd Atlantic injection	145.0
3rd Atlantic injection (same tracking as for 2nd Atlantic injection plus the adjacent)	CYI CRO CAL WHS EGL CNV BDA <sup>b</sup>	98.9 - 102.4 135.6 - 136.2 169.2 - 171.5 171.1 - 175.2 175.3 - 179.3 177.0 - 180.4 180.0 - 184.1	218.5
3rd Pacific injection	Same as for 3rd Atlantic injection	Same as for 3rd Atlantic injection	232.5

<sup>a</sup> Injection opportunity does not meet the 30 - 90 minute update criteria.

<sup>b</sup> Update occurred over the station.

TABLE A-II.- TRACKING VISIBILITY PROFILE - Concluded

Injection opportunity	Station	Tracking interval, minutes past earth parking orbit insertion	Injection, minutes past earth parking orbit insertion
(d) -27.5 Lunar declination, 108° launch azimuth			
1st Atlantic injection <sup>a</sup>	---	---	---
1st Pacific injection <sup>a</sup>	---	---	---
2nd Atlantic injection	ANT ASC PRE CRO GUA <sup>b,c</sup>	0.0 - 1.1 10.7 - 14.7 22.3 - 25.9 42.4 - 44.1 54.4 - 56.0	85.0
2nd Pacific injection (same tracking as for 2nd Atlantic injection plus the adjacent)	CAL WHS <sup>b,c</sup> TEX	75.2 - 79.2 78.3 - 82.2 81.0 - 84.5	157.5
3rd Atlantic injection (same tracking as for 2nd Pacific injection plus the adjacent)	EGL GTI PRE GUA <sup>b,c</sup>	84.0 - 84.5 87.8 - 89.5 115.6 - 117.5 145.4 - 149.0	172.5
3rd Pacific injection (same tracking as for 3rd Atlantic injection plus the adjacent)	CAL <sup>b,c</sup> GYM <sup>b,c</sup>	168.4 - 169.8 170.1 - 173.4	244.5

<sup>a</sup>Injection opportunity does not meet the 30 - 90 minute update criteria.

<sup>b</sup>Update occurred over the station.

<sup>c</sup>No C-band tracking.

TABLE A-III.- ERROR MODEL ASSUMED FOR THE GROUND NAVIGATION SYSTEM.<sup>a</sup>

Radar	Type	Bias			Noise			Station location uncertainties		
		Azimuth angle, m. rad	Elevation angle, m. rad	Range, ft	Azimuth angle, m. rad	Elevation angle, m. rad	Range, ft	$\sigma_x$ , ft	$\sigma_y$ , ft	$\sigma_z$ , ft
CYI	MPS-26	1.0	1.0	60	2.0	2.0	120	105	458	466
CRO	FPQ-6	0.15	0.15	20	0.3	0.3	40	216	202	192
WHS	FPS-16	0.2	0.2	30	0.4	0.4	60	131	103	101
EGL	FPS-16	0.2	0.2	30	0.4	0.4	60	131	105	101
CNV	FPS-16	0.2	0.2	30	0.4	0.4	60	131	107	101
GBI	FPS-16	0.2	0.2	30	0.4	0.4	60	134	109	101
BDA	FPQ-6	0.15	0.15	20	0.3	0.3	40	141	120	122
CAL	FPS-16	0.2	0.2	30	0.4	0.4	60	131	100	101
HAW	FPS-16	0.2	0.2	30	0.4	0.4	60	141	150	142
ANT	FPQ-6	0.15	0.15	20	0.3	0.3	40	138	116	112
ASC	FPS-16	0.2	0.2	30	0.4	0.4	60	105	352	345
PRE	MPS-25	1.0	1.0	60	2.0	2.0	120	141	137	142
GTI	TPQ-18	0.2	0.2	30	0.4	0.4	60	138	113	101

<sup>a</sup>Uncertainty in gravitational constant of earth =  $1.06 \times 10^{11} \text{ ft}^3/\text{sec}^2$ Uncertainty in acceleration due to venting =  $1.1428 \times 10^{-4} \text{ ft/sec}^2$ Uncertainty in drag = 10 percent of total drag =  $1.465 \times 10^{-6} \text{ ft/sec}^2$

TABLE A-IV.- COVARIANCE MATRICES OF IU ESTIMATE AT EPOI FOR VARIOUS LAUNCH AZIMUTHS

72.6° Launch azimuth

0.244434E 06	-0.186499E 06	-0.790528E 03	0.983913E 03	-0.515144E 03	-0.377653E 01
-0.186499E 06	0.185955E 06	0.373498E 03	-0.780784E 03	0.490326E 03	0.223698E 01
-0.790528E 03	0.373498E 03	0.295004E 06	-0.459138E 01	0.134469E 01	0.874968E 03
0.983913E 03	-0.780784E 03	-0.459138E 01	0.404943E 01	-0.216422E 01	-0.192262E-01
-0.515144E 03	0.490326E 03	0.134469E 01	-0.216422E 01	0.132271E 01	0.709504E-02
-0.377653E 01	0.223698E 01	0.874968E 03	-0.192262E-01	0.709504E-02	0.275595E 01

90° Launch azimuth

0.259309E 06	-0.183551E 06	-0.804892E 03	0.103513E 04	-0.493244E 03	-0.386334E 01
-0.183551E 06	0.171079E 06	0.341444E 03	-0.758883E 03	0.439111E 03	0.208348E 01
-0.804892E 03	0.341444E 03	0.295004E 06	-0.464169E 01	0.115918E 01	0.874968E 03
0.103513E 04	-0.758883E 03	-0.464169E 01	0.421875E 01	-0.204780E 01	-0.194956E-01
-0.493244E 03	0.439111E 03	0.115918E 01	-0.204780E 01	0.115339E 01	0.631706E-02
-0.386334E 01	0.208348E 01	0.874968E 03	-0.194956E-01	0.631706E-02	0.275595E 01

108° Launch azimuth

0.245696E 06	-0.186297E 06	-0.791788E 03	0.988295E 03	-0.513458E 03	-0.378409E 01
-0.186297E 06	0.184692E 06	0.370819E 03	-0.779098E 03	0.485944E 03	0.222418E 01
-0.791788E 03	0.370819E 03	0.295004E 06	-0.459591E 01	0.132913E 01	0.874968E 03
0.988295E 03	-0.779098E 03	-0.459591E 01	0.406406E 01	-0.215494E 01	-0.192501E-01
-0.513458E 03	0.485944E 03	0.132913E 01	-0.215494E 01	0.130808E 01	0.702990E-02
-0.378409E 01	0.222418E 01	0.874968E 03	-0.192501E-01	0.702990E-02	0.275595E 01

TABLE A-V.- FORMAT OF THE COVARIANCE MATRICES AT  
THE START OF THE TLI MANEUVER

Time of TLI, minutes after EPOI	Approximate time of vector update (if applicable), minutes after EPOI (a, b)	Navigation system considered and covariance matrix number	
		IU	Ground and IU or Ground and CM (b)
72.6° Launch azimuth; +27.5° lunar declination			
131.0	90.0	1	17
145.0	90.0	2	18
218.5	180.0	3	19
232.5	180.0	4	20
72.6° Launch azimuth; -27.5° lunar declination			
86.0	50.0	5	21
101.0	50.0	6	22
173.0	136.0	7	23
188.5	136.0	8	24
260.5	228.0	9	25
90° Launch azimuth; -27.5° lunar declination			
168.0	135.0	10	26
176.0	135.0	11	27
256.0	197.0	12	28
108° Launch azimuth; -27.5° lunar declination			
85.0	55.0	13	29
157.5	83.0	14	30
172.5	147.0	15	31
244.5	172.0	16	32

<sup>a</sup>See table A-II for ground track profile.

<sup>b</sup>The update was uplinked to the CM at this time, but the values were those predicted by the ground navigation system to the start of TLI.

TABLE A-VI.- COVARIANCE MATRIX AT THE START OF TL<sub>1</sub><sup>a</sup>

## Number

## Covariance Matrix

		Covariance Matrix															
		Number															
		(1,1)-0.81194400E 07	(1,2)-0.44523000E 08	(1,3)-0.19418400E 04	(1,4) 0.56904300E 05	(1,5)-0.76497100E 04	(1,6)-0.12221700E 02										
		(1,2,1)-0.44523000E 08	(2,3)-0.48928000E 04	(2,4) 0.32882900E 06	(2,5) 0.36525000E 05	(2,6) 0.28105900E 01											
1		(3,1)-0.15418400E 04	(3,2)-0.48928000E 04	(3,3) 0.27619100E 06	(3,4) 0.18821800E 01	(3,5) 0.19552100E 01	(3,6) 0.844921700E 03										
		(4,1,1) 0.56904300E 05	(4,2)-0.32829000E 06	(4,3) 0.18821800E 01	(4,4) 0.40955100E 03	(4,5)-0.47012100E 02	(4,6) 0.20173500E-01										
		(5,1)-0.74697100E 04	(5,2) 0.36525000E 05	(5,3) 0.19552100F 01	(5,4)-0.47012100E 02	(5,5) 0.67790900E 01	(5,6) 0.12055500E-01										
		(6,1)-0.12221700E 02	(6,2) 0.28105900E 01	(6,3) 0.844921700E 04	(6,4)-0.20173500E-01	(6,5) 0.12055500E-01	(6,6) 0.27829200E 01										
		(1,1,1) 0.11100200E CB	(1,1,2)-0.64524280CE 08	(1,1,3)-0.16568100E 05	(1,1,4) 0.75149500E 05	(1,1,5)-0.97844200E 04	(1,1,6)-0.67108600E 01										
		(1,2,1)-0.64523000E CB	(1,2,2) 0.45543200E 09	(1,2,3) 0.25928400E 05	(1,2,4)-0.53270400F 06	(1,2,5) 0.53188600E 05	(1,2,6) 0.17750400E 02										
		(1,3,1)-0.14523000E C5	(1,3,2) 0.25923600E 05	(1,3,3) 0.21015139CE 07	(1,3,4)-0.32147000E 02	(1,3,5) 0.17822500E 02	(1,3,6) 0.53904900E 03										
2		(1,4,1) 0.75149500E C5	(1,4,2)-0.53270400E 05	(1,4,3) 0.62147000E 02	(1,4,4) 0.52366800F 03	(1,4,5)-0.62149300E 02	(1,4,6) 0.20963500E-01										
		(1,5,1)-0.97844200E C5	(1,5,2) 0.53182500E 05	(1,5,3) 0.17822500E 02	(1,5,4)-0.62149300E 02	(1,5,5) 0.89646500E 01	(1,5,6) 0.70212100E-02										
		(1,6,1)-0.67108600E 01	(1,6,2) 0.17750400E 02	(1,6,3) 0.53904900E 03	(1,6,4)-0.20963500F-01	(1,6,5) 0.70216000E-02	(1,6,6) 0.16054900E 00										
		(1,1,1) 0.12946000E CR	(1,1,2)-0.12950500CE C9	(1,1,3)-0.19861200F 04	(1,1,4) 0.15837300E 06	(1,1,5)-0.19067700F 05	(1,1,6)-0.12259600E 02										
		(1,2,1)-0.12895000E CS	(1,2,2) 0.13202900E 10	(1,2,3) 0.12553600E 06	(1,2,4)-0.16696300E 07	(1,2,5) 0.96245200E 05	(1,2,6) 0.45537000E 02										
		(1,3,1)-0.16118000E C9	(1,2,1) 0.18515500E 09	(1,2,3) 0.578174300F 05	(1,2,4)-0.22077000E 07	(1,2,5) 0.22256100E 06	(1,2,6) 0.33410400E 02										
		(1,4,1)-0.19817200E C4	(1,2,1) 0.105523600E 04	(1,3,3) 0.28083300E 01	(1,3,4)-0.528833300E 01	(1,3,5) 0.20012100E 01	(1,3,6) 0.85570600E 03										
		(1,5,1)-0.15873000E C6	(1,4,2)-0.16598300E 07	(1,4,3)-0.528883300E 01	(1,4,4) 0.20363390CE 01	(1,4,5)-0.18896200E 03	(1,4,6) 0.68821500E-01										
		(1,6,1)-0.106167700E C5	(1,5,2) 0.96429700E 05	(1,5,3) 0.20012100E 01	(1,5,4) 0.11896200F 03	(1,5,5) 0.87344000E 01	(1,5,6) 0.12102300E-01										
		(1,6,1)-0.12229600E C2	(1,6,2) 0.43537000E 02	(1,6,3) 0.855570600E 03	(1,6,4)-0.68821500E-01	(1,6,5) 0.12102300E-01	(1,6,6) 0.27762600E 01										
		(1,1,1) 0.15692600E CB	(1,1,2)-0.16119000E C9	(1,1,3)-0.165889900E 05	(1,1,4) 0.19174000E 06	(1,1,5)-0.12668200E 05	(1,1,6)-0.664452400E 01										
		(1,2,1)-0.16118000E C9	(1,2,2) 0.18515500E 09	(1,2,3) 0.578174300F 05	(1,2,4)-0.22077000E 07	(1,2,5) 0.22256100E 06	(1,2,6) 0.33410400E 02										
		(1,3,1)-0.16118000E C5	(1,3,2) 0.578174300E 05	(1,3,3) 0.210151390F 07	(1,3,4)-0.70346800E 02	(1,3,5) 0.17845100E 02	(1,3,6) 0.53120700E 03										
		(1,4,1)-0.19817200E C4	(1,2,1) 0.105523600E 04	(1,3,3) 0.28083300E 01	(1,3,4)-0.528833300E 01	(1,3,5) 0.20012100E 03	(1,3,6) 0.85570600E 03										
		(1,5,1)-0.15873000E C6	(1,4,2)-0.16598300E 07	(1,4,3)-0.528883300E 01	(1,4,4) 0.20363390CE 01	(1,4,5)-0.18896200E 03	(1,4,6) 0.68821500E-01										
		(1,6,1)-0.66524000E C1	(1,6,2) 0.33410400F 02	(1,6,3) 0.53120700F 03	(1,6,4)-0.39691300E-01	(1,6,5) 0.65847000E-02	(1,6,6) 0.15636600E 00										
		(1,1,1) 0.128890CE 07	(1,1,2)-0.215561700E 07	(1,1,3)-0.21969300F 03	(1,1,4) 0.31710600F 04	(1,1,5)-0.92021200F 03	(1,1,6)-0.23311000E 01										
		(1,2,1)-0.21551700F 07	(1,2,2) 0.17798700F 08	(1,2,3)-0.17798700F 08	(1,2,4)-0.17798700F 08	(1,2,5) 0.17798700F 08	(1,2,6) 0.33410400E 02										
		(1,3,1)-0.21969300E 03	(1,3,2) 0.26126000E 04	(1,3,3) 0.16109500F 06	(1,3,4) 0.31096100E 06	(1,3,5) 0.43684200E 06	(1,3,6) 0.653179800E 03										
		(1,4,1)-0.31770600E 04	(1,4,2)-0.31771100E 06	(1,4,3)-0.337996700E 06	(1,4,4) 0.157858500E 03	(1,4,5) 0.67019300E 01	(1,4,6) 0.295572100E-01										
		(1,5,1)-0.92121200E C3	(1,5,2) 0.12226100E 06	(1,5,3) 0.17845100CE 02	(1,5,4) 0.434848200E 00	(1,5,5) 0.61019300E 01	(1,5,6) 0.13724500E 01										
		(1,6,1)-0.23311000E C1	(1,6,2) 0.33410400F 02	(1,6,3) 0.53120700F 03	(1,6,4)-0.39691300E-01	(1,6,5) 0.65847000E-02	(1,6,6) 0.27762600E 01										
		(1,1,1) 0.22269400F 07	(1,1,2)-0.465958700E 07	(1,1,3)-0.975307799E 04	(1,1,4) 0.57050800E 04	(1,1,5)-0.22717200E 04	(1,1,6)-0.358177500E 01										
		(1,2,1)-0.465958700E 07	(1,2,2) 0.11151700F 08	(1,2,3)-0.13991200E 05	(1,2,4)-0.13991200E 05	(1,2,5) 0.42295800E 06	(1,2,6) 0.93329099E 01										
		(1,3,1)-0.219537099E 04	(1,3,2)-0.13993200E 05	(1,3,3) 0.15340900F 07	(1,3,4) 0.70861400E 07	(1,3,5) 0.13678800E 07	(1,3,6) 0.567752300E 03										
		(1,4,1) 0.57050800E 04	(1,4,2)-0.14461800E 06	(1,4,3) 0.15343900F 07	(1,4,4) 0.19022300E 03	(1,4,5) 0.567752300E 01	(1,4,6) 0.11315500E-01										
		(1,5,1)-0.22717200E 04	(1,5,2)-0.422958700E 05	(1,5,3) 0.13678800E 02	(1,5,4) 0.756792300E 01	(1,5,5) 0.31056400E 01	(1,5,6) 0.534625300E-02										
		(1,6,1)-0.358177500E C1	(1,6,2)-0.93329099E 01	(1,6,3) 0.58545500E 03	(1,6,4)-0.111315500E-01	(1,6,5) 0.53425300E-02	(1,6,6) 0.18593000E 00										

a Locate the covariance matrix number on table A-V for a description of the events preceding TL1.

TABLE A-VI. - Continued a

Covariance Matrix											
Number	(1,1)	(1,2)	(1,3)	(1,4)	(1,5)	(1,6)	(1,7)	(1,8)	(1,9)	(1,10)	(1,11)
7	(1,1) 0.41037200E 07 (1,2) -0.32745700E 08 (1,3) -0.03975200E 02 (1,4) 0.39735700E 05 (1,5) -0.26800800E 04 (1,6) -0.18438500E 01										
8	(1,1) 0.53276300E 07 (1,2) -0.385922500E 08 (1,3) -0.97665689E 04 (1,4) 0.46374299E 05 (1,5) -0.40212000E 04 (1,6) -0.39431199E 01										
9	(1,1) 0.91299400E 07 (1,2) -0.11934600E 09 (1,3) -0.10353500E 03 (1,4) 0.14342300E 06 (1,5) -0.57007100E 04 (1,6) -0.16931900E 01										
10	(1,1) 0.40568000E 07 (1,2) -0.38777200E 09 (1,3) -0.58178700E 03 (1,4) 0.115889700E 05 (1,5) -0.24631000E 04 (1,6) -0.38379300E 01										
11	(1,1) 0.43869000E 07 (1,2) -0.31782300E 08 (1,3) -0.13988200E 04 (1,4) 0.38975100E 05 (1,5) -0.30505500E 04 (1,6) -0.46381200E 01										
12	(1,1) 0.406532500E 07 (1,2) -0.122598200E 09 (1,3) -0.35731500E 03 (1,4) 0.15747100E 06 (1,5) -0.54893700E 04 (1,6) -0.32343900E 01										
13	(1,1) -0.32735700E 08 (1,2) -0.78266600E 09 (1,3) -0.91759000E 04 (1,4) 0.12570000E 06 (1,5) -0.42215200E 02 (1,6) -0.25715800E 02										
14	(1,1) 0.15047100E 06 (1,2) -0.28722800E 07 (1,3) -0.622215200E 02 (1,4) 0.339339200E 04 (1,5) -0.76633300E 02 (1,6) -0.57835400E 03										
15	(1,1) 0.39735700E 05 (1,2) -0.91125900E 06 (1,3) -0.16607500E 01 (1,4) 0.10633999E 04 (1,5) -0.57862000E 01 (1,6) -0.78359200E 01										
16	(1,1) -0.26800800E 04 (1,2) 0.36266400E 04 (1,3) 0.21307800E 00 (1,4) 0.57662000E 01 (1,5) 0.23741000E 01 (1,6) 0.6218200E 02										
17	(1,1) 0.39735700E 05 (1,2) -0.91125900E 06 (1,3) -0.16607500E 01 (1,4) 0.10633999E 04 (1,5) -0.57862000E 01 (1,6) -0.78359200E 01										
18	(1,1) -0.18438500E 01 (1,2) -0.81106700E 02 (1,3) 0.57835400E 03 (1,4) 0.78859200E 01 (1,5) 0.48212000E 02 (1,6) 0.249931500E 01										
19	(1,1) 0.41037200E 07 (1,2) -0.32745700E 08 (1,3) -0.03975200E 02 (1,4) 0.39735700E 05 (1,5) -0.26800800E 04 (1,6) -0.18438500E 01										
20	(1,1) 0.53276300E 07 (1,2) -0.385922500E 08 (1,3) -0.97665689E 04 (1,4) 0.46374299E 05 (1,5) -0.40212000E 04 (1,6) -0.39431199E 01										
21	(1,1) 0.91299400E 07 (1,2) -0.11934600E 09 (1,3) -0.10353500E 03 (1,4) 0.14342300E 06 (1,5) -0.57007100E 04 (1,6) -0.16931900E 01										
22	(1,1) 0.40568000E 07 (1,2) -0.38777200E 08 (1,3) -0.58178700E 03 (1,4) 0.115889700E 05 (1,5) -0.24631000E 04 (1,6) -0.38379300E 01										
23	(1,1) -0.10535000E 03 (1,2) -0.50391100E 06 (1,3) 0.13051100E 01 (1,4) 0.37053000E 02 (1,5) 0.23382400E 00 (1,6) -0.33765300E 01										
24	(1,1) -0.14343300E 06 (1,2) -0.747172000E 07 (1,3) 0.236066800E 01 (1,4) 0.388618200E 02 (1,5) -0.25287300E 02 (1,6) 0.48804900E 00										
25	(1,1) 0.44666800E 05 (1,2) 0.477097100E 04 (1,3) 0.233324200E 00 (1,4) -0.58287300E 02 (1,5) 0.41946600E 01 (1,6) -0.29965300E 02										
26	(1,1) -0.577097100E 03 (1,2) -0.12221600E 03 (1,3) 0.577686600E 03 (1,4) 0.30958900E 01 (1,5) 0.528855300E 02 (1,6) 0.18236500E 00										
27	(1,1) -0.18438500E 01 (1,2) -0.81106700E 02 (1,3) 0.57835400E 03 (1,4) 0.78859200E 01 (1,5) 0.48212000E 02 (1,6) 0.249931500E 01										
28	(1,1) 0.41037200E 07 (1,2) -0.32745700E 08 (1,3) -0.03975200E 02 (1,4) 0.39735700E 05 (1,5) -0.26800800E 04 (1,6) -0.18438500E 01										
29	(1,1) 0.53276300E 07 (1,2) -0.385922500E 08 (1,3) -0.97665689E 04 (1,4) 0.46374299E 05 (1,5) -0.40212000E 04 (1,6) -0.39431199E 01										
30	(1,1) 0.91299400E 07 (1,2) -0.11934600E 09 (1,3) -0.10353500E 03 (1,4) 0.14342300E 06 (1,5) -0.57007100E 04 (1,6) -0.16931900E 01										
31	(1,1) 0.40568000E 07 (1,2) -0.38777200E 08 (1,3) -0.58178700E 03 (1,4) 0.115889700E 05 (1,5) -0.24631000E 04 (1,6) -0.38379300E 01										
32	(1,1) -0.38777200E 08 (1,2) 0.65710400E 09 (1,3) 0.15588300E 05 (1,4) -0.10416400E 06 (1,5) 0.15627000E 01 (1,6) -0.49023300E 02										
33	(1,1) -0.10535000E 03 (1,2) -0.50391100E 06 (1,3) 0.13051100E 01 (1,4) 0.37053000E 02 (1,5) 0.23382400E 00 (1,6) -0.33765300E 01										
34	(1,1) 0.44666800E 05 (1,2) 0.477097100E 04 (1,3) 0.233324200E 00 (1,4) -0.58287300E 02 (1,5) 0.41946600E 01 (1,6) -0.29965300E 02										
35	(1,1) -0.29545600E 02 (1,2) -0.75287300E 03 (1,3) 0.577686600E 02 (1,4) -0.178929800E 03 (1,5) -0.25287300E 02 (1,6) 0.3102900E 01										
36	(1,1) -0.18438500E 01 (1,2) -0.81106700E 02 (1,3) 0.57835400E 03 (1,4) 0.78859200E 01 (1,5) 0.48212000E 02 (1,6) 0.249931500E 01										
37	(1,1) 0.41037200E 07 (1,2) -0.32745700E 08 (1,3) -0.03975200E 02 (1,4) 0.39735700E 05 (1,5) -0.26800800E 04 (1,6) -0.18438500E 01										
38	(1,1) 0.53276300E 07 (1,2) -0.385922500E 08 (1,3) -0.97665689E 04 (1,4) 0.46374299E 05 (1,5) -0.40212000E 04 (1,6) -0.39431199E 01										
39	(1,1) 0.91299400E 07 (1,2) -0.11934600E 09 (1,3) -0.10353500E 03 (1,4) 0.14342300E 06 (1,5) -0.57007100E 04 (1,6) -0.16931900E 01										
40	(1,1) 0.40568000E 07 (1,2) -0.38777200E 08 (1,3) -0.58178700E 03 (1,4) 0.115889700E 05 (1,5) -0.24631000E 04 (1,6) -0.38379300E 01										
41	(1,1) -0.10535000E 03 (1,2) -0.50391100E 06 (1,3) 0.13051100E 01 (1,4) 0.37053000E 02 (1,5) 0.23382400E 00 (1,6) -0.33765300E 01										
42	(1,1) 0.44666800E 05 (1,2) 0.477097100E 04 (1,3) 0.233324200E 00 (1,4) -0.58287300E 02 (1,5) 0.41946600E 01 (1,6) -0.29965300E 02										
43	(1,1) -0.29545600E 02 (1,2) -0.75287300E 03 (1,3) 0.577686600E 02 (1,4) -0.178929800E 03 (1,5) -0.25287300E 02 (1,6) 0.3102900E 01										
44	(1,1) -0.18438500E 01 (1,2) -0.81106700E 02 (1,3) 0.57835400E 03 (1,4) 0.78859200E 01 (1,5) 0.48212000E 02 (1,6) 0.249931500E 01										
45	(1,1) 0.41037200E 07 (1,2) -0.32745700E 08 (1,3) -0.03975200E 02 (1,4) 0.39735700E 05 (1,5) -0.26800800E 04 (1,6) -0.18438500E 01										
46	(1,1) 0.53276300E 07 (1,2) -0.385922500E 08 (1,3) -0.97665689E 04 (1,4) 0.46374299E 05 (1,5) -0.40212000E 04 (1,6) -0.39431199E 01										
47	(1,1) 0.91299400E 07 (1,2) -0.11934600E 09 (1,3) -0.10353500E 03 (1,4) 0.14342300E 06 (1,5) -0.57007100E 04 (1,6) -0.16931900E 01										
48	(1,1) 0.40568000E 07 (1,2) -0.38777200E 08 (1,3) -0.58178700E 03 (1,4) 0.115889700E 05 (1,5) -0.24631000E 04 (1,6) -0.38379300E 01										
49	(1,1) -0.10535000E 03 (1,2) -0.50391100E 06 (1,3) 0.13051100E 01 (1,4) 0.37053000E 02 (1,5) 0.23382400E 00 (1,6) -0.33765300E 01										
50	(1,1) 0.44666800E 05 (1,2) 0.477097100E 04 (1,3) 0.233324200E 00 (1,4) -0.58287300E 02 (1,5) 0.41946600E 01 (1,6) -0.29965300E 02										
51	(1,1) -0.29545600E 02 (1,2) -0.75287300E 03 (1,3) 0.577686600E 02 (1,4) -0.178929800E 03 (1,5) -0.25287300E 02 (1,6) 0.3102900E 01										
52	(1,1) -0.18438500E 01 (1,2) -0.81106700E 02 (1,3) 0.57835400E 03 (1,4) 0.78859200E 01 (1,5) 0.48212000E 02 (1,6) 0.249931500E 01										
53	(1,1) 0.41037200E 07 (1,2) -0.32745700E 08 (1,3) -0.03975200E 02 (1,4) 0.39735700E 05 (1,5) -0.26800800E 04 (1,6) -0.18438500E 01										
54	(1,1) 0.53276300E 07 (1,2) -0.385922500E 08 (1,3) -0.97665689E 04 (1,4) 0.46374299E 05 (1,5) -0.40212000E 04 (1,6) -0.39431199E 01										
55	(1,1) 0.91299400E 07 (1,2) -0.11934600E 09 (1,3) -0.10353500E 03 (1,4) 0.14342300E 06 (1,5) -0.57007100E 04 (1,6) -0.16931900E 01										
56	(1,1) 0.40568000E 07 (1,2) -0.38777200E 08 (1,3) -0.58178700E 03 (1,4) 0.115889700E 05 (1,5) -0.24631000E 04 (1,6) -0.38379300E 01										
57	(1,1) -0.10535000E 03 (1,2) -0.50391100E 06 (1,3) 0.13051100E 01 (1,4) 0.37053000E 02 (1,5) 0.23382400E 00 (1,6) -0.33765300E 01										
58	(1,1) 0.44666800E 05 (1,2) 0.477097100E 04 (1,3) 0.233324200E 00 (1,4) -0.58287300E 02 (1,5) 0.41946600E 01 (1,6) -0.29965300E 02										
59	(1,1) -0.29545600E 02 (1,2) -0.75287300E 03 (1,3) 0.577686600E 02 (1,4) -0.178929800E 03 (1,5) -0.25287300E 02 (1,6) 0.3102900E 01										
60	(1,1) -0.18438500E 01 (1,2) -0.81106700E 02 (1,3) 0.57835400E 03 (1,4) 0.78859200E 01 (1,5) 0.48212000E 02 (1,6) 0.249931500E 01										
61	(1,1) 0.41037200E 07 (1,2) -0.32745700E 08 (1,3) -0.03975200E 02 (1,4) 0.39735700E 05 (1,5) -0.26800800E 04 (1,6) -0.18438500E 01										
62	(1,1) 0.53276300E 07 (1,2) -0.385922500E 08 (1,3) -0.97665689E 04 (1,4) 0.46374299E 05 (1,5) -0.40212000E 04 (1,6) -0.39431199E 01										
63	(1,1) 0.91299400E 07 (1,2) -0.11934600E 09 (1,3) -0.10353500E 03 (1,4) 0.14342300E 06 (1,5) -0.57007100E 04 (1,6) -0.16931900E 01										
64	(1,1) 0.40568000E 07 (1,2) -0.38777200E 08 (1,3) -0.58178700E 03 (1,4) 0.115889700E 05 (1,5) -0.24631000E 04 (1,6) -0.38379300E 01										
65	(1,1) -0.10535000E 03 (1,2) -0.50391100E 06 (1,3) 0.13051100E 01 (1,4) 0.37053000E 02 (1,5) 0.23382400E 00 (1,6) -0.33765300E 01										
66	(1,1) 0.44666800E 05 (1,2) 0.477097100E 04 (1,3) 0.233324200E 00 (1,4) -0.58287300E 02 (1,5) 0.41946600E 01 (1,6) -0.29965300E 02										
67	(1,1) -0.29545600E 02 (1,2) -0.75287300E 03 (1,3) 0.577686600E 02 (1,4) -0.178929800E 03 (1,5) -0.25287300E 02 (1,6) 0.3102900E 01										
68	(1,1) -0.18438500E 01 (1,2) -0.81106700E 02 (1,3) 0.57835400										

TABLE A-VI. - Continued a

## Covariance Matrix

Number	(1,1) 0.11674700E 07	(1,2)-0.20036700E 07	(1,3) 0.21448800E 02	(1,4) 0.37938300E 04	(1,5)-0.80281300E 03	(1,6)-0.12453100E 01
	+2.771-0.28536700E C7	-1.271-0.72672800E C7	-12.31-0.14116600E 03	-12.31-0.14116600E 03	-12.31-0.13520500E 06	-12.5-0.58785100E 04
13	(3,1) 0.21448800E 02	(3,2)-0.14116600E 03	(3,3) 0.92672000E 05	(3,4)-0.15142400E 01	(3,5)-0.16661600E-01	(3,6) 0.48460300E 03
	+4.1-0.3939300E 04	+4.2-0.3939300E 04	+4.3-0.15142400E 01	(4,4) 0.15151600E 03	(4,5) 0.5671300E 01	0.2005000E-01
	(5,1)-0.80281300E 03	(5,2)-0.5671300E 01	(5,3)-0.16661600E-01	(5,4) 0.56741300E 01	(5,5) 0.11676400E 01	(5,6) 0.40312100E-02
	+6.1-0.2453100E 01	+6.2-0.12453100E 01	+6.3-0.56741300E 01	+6.4) 0.2453100E 03	+6.5-0.40312100E-02	+6.6) 0.30495500E 01
14	(1,1) 0.66746100E 07	(1,2)-0.57699000E 07	(1,3) 0.10653000E 05	(1,4) 0.65871000E 05	(1,5)-0.48754400E 04	(1,6) 0.861536400E 01
	(2,1)-0.516994800E 04	(2,2) 0.6511600E 09	(2,3) 0.466772000E 05	(2,4)-0.72402800E 06	(2,5) 0.29901300E 02	
	(3,1)-0.16661600E C5	(3,2) 0.42565500E 05	(3,3) 0.122465500E 07	(3,4)-0.47902000E 02	(3,5) 0.1095700E 02	
	(4,1) 0.65971000E 05	(4,2)-0.27402800E 05	(4,3) 0.47902000E 02	(4,4) 0.82773300E 03	(4,5) 0.44424700E 02	(4,6) 0.27987500E 04
	+5.1-0.2453100E 04	+5.2-0.12453100E 04	+5.3-0.47902000E 02	+5.4-0.44424700E 02	+5.5-0.3777000E 07	+5.6-0.90973400E-02
	(6,1) 0.861536400E 01	(6,2)-0.299001300E 02	(6,3)-0.12453100E 04	(6,4) 0.29987500E-01	(6,5) 0.12796200E 01	
15	(1,1) 0.49759100E 07	(1,2)-0.33487000E 07	(1,3) 0.133302900E 02	(1,4) 0.46379700E 05	(1,5)-0.26259200E 04	(1,6)-0.12941600E 01
	+2.771-0.33349700E C7	+2.71-0.77737300E C7	+2.31-0.11375000E 05	+2.41-0.89755500E 06	+2.51 0.47927000E 04	+2.61-0.78972000E 02
	(3,1) 0.13230200E 02	(3,2)-0.427561100E 03	(3,3) 0.95136500E 05	(3,4)-0.11376000E 01	(3,5)-0.16312100E 04	(3,6) 0.49233400E 03
	+4.1-0.43779700E 05	+4.2-0.13375000E 06	+4.3-0.11376000E 01	+4.4-0.314694400E 04	+4.5-0.71112900E 01	+4.6) 0.73927100E-01
	(5,1)-0.26259200E 04	(5,2) 0.47927000E 04	(5,3)-0.16312100E 04	(5,4) 0.11942700E 01	(5,5) 0.22664100E 01	(5,6) 0.4092500E-02
	+6.1-0.12961600E 01	+6.2-0.78972000E 01	+6.3-0.427561100E 03	+6.4) 0.759477000E-01	+6.5-0.4092500E-02	+6.6) 0.30922300E 01
16	(1,1) 0.11716500E 08	(1,2)-0.15301700E 09	(1,3) 0.11167000E 05	(1,4) 0.18000800E 06	(1,5)-0.80957800E 04	(1,6) 0.83931600E 01
	(2,1)-0.15301700E C9	(2,2) 0.2292500E 01	(2,3) 0.866000E 05	(2,4)-0.26798500E 07	(2,5) 0.10201500E 06	(2,6) 0.45508300E 02
	(3,1)-0.11716500E 05	(3,2) 0.78650800E 05	(3,3) 0.13041500E 07	(3,4)-0.83832900E 02	(3,5) 0.1147832900E 04	(3,6) 0.26397000E 04
	(4,1) 0.14068400E 06	(4,2)-0.26798500E 06	(4,3) 0.83832900E 02	(4,4) 0.314694400E 04	(4,5) 0.19427000E 03	(4,6) 0.47335300E-01
	+5.1-0.89378000E 06	+5.2-0.10701500E 06	+5.3-0.77478000E 02	+5.4-0.11942700E 03	+5.5-0.35332900E 01	+5.6) 0.85043400E-02
	(6,1) 0.83931600E 01	(6,2)-0.45508300E 02	(6,3)-0.12639700E 04	(6,4) 0.47335300E-01	(6,5) 0.89043400E-02	(6,6) 0.11799600E 01
17	(1,1) 0.15616700E 07	(1,2)-0.49015500E 07	(1,3) 0.111542100E 05	(1,4) 0.577918200E 04	(1,5)-0.11596100E 04	(1,6)-0.20289700E 03
	(2,1)-0.49015500E 07	(2,2) 0.16166100E 08	(2,3) 0.68236900E 05	(2,4) 0.19059100E 05	(2,5) 0.36772000E 04	(2,6) 0.60466600E 03
	(3,1) 0.15631000E 05	(3,2)-0.68236900E 05	(3,3) 0.20009400E 05	(3,4) 0.79241600E 02	(3,5) 0.33744800E 03	(3,6) 0.4866900E 02
	(4,1) 0.57918200E 04	(4,2)-0.19059100E 05	(4,3) 0.79241600E 02	(4,4) 0.22478800E 02	(4,5) 0.43456000E 01	(4,6) 0.71319200E 00
	(5,1)-0.15616700E 04	(5,2) 0.36772000E 04	(5,3) 0.33744800E 01	(5,4) 0.43456000E 01	(5,5) 0.3843000E 00	(5,6) 0.15525700E 00
	(6,1)-0.20289700E 03	(6,2) 0.60466600E 03	(6,3) 0.45508300E 02	(6,4) 0.71319200E 00	(6,5) 0.16525700E 00	(6,6) 0.26623100E 00
18	(1,1) 0.12110900E C7	(1,2)-0.64042900E 07	(1,3) 0.49940700E 05	(1,4) 0.73286200E 04	(1,5)-0.75876900E 03	(1,6) 0.88928000E 02
	(2,1)-0.64042900E 07	(2,2) 0.33892400E 08	(2,3) 0.244575200E 06	(2,4)-0.38782290E 05	(2,5) 0.39476300E 04	(2,6) 0.67770700E 03
	(3,1) 0.12110900E 05	(3,2)-0.33892400E 05	(3,3) 0.13165500F 05	(3,4) 0.26877500E 03	(3,5) 0.40056800E 02	(3,6) 0.5646200E 02
	(4,1) 0.73286200E 04	(4,2)-0.38782290E 05	(4,3) 0.22478800E 02	(4,4) 0.45517200E 02	(4,5) 0.52378600E 01	
	(5,1)-0.75876900E 03	(5,2) 0.39476300E 04	(5,3) 0.40056800E 02	(5,4) 0.47796900E 01	(5,5) 0.5258600E-01	
	(6,1)-0.88928000E 02	(6,2) 0.54646200E 03	(6,3) 0.54646200E 02	(6,4)-0.54377000E 02	(6,5) 0.42583800E-01	

a Locate the covariance matrix number on table A-V for a description  
of the events preceding TLI.

TABLE A-VI. - Continued a

## Covariance Matrix

Number	Covariance Matrix											
19	(1,1) 0.2347689E-02 (1,2)-0.3608080E-07 (1,3)-0.12426900E-06 (1,4) 0.51065100E-04 (1,5)-0.17837100E-04 (1,6)-0.2145800E-02	(1,1) 0.42330100E-07 (1,2)-0.10448200E-08 (1,3)-0.110680400E-06 (1,4) 0.1291000E-05 (1,5)-0.34936100E-04 (1,6) 0.15578800E-03	(1,1) 0.10448200E-08 (1,2) 0.25925700E-08 (1,3) 0.15569200E-06 (1,4) 0.66388800E-06 (1,5) 0.22915300E-04 (1,6) 0.34663000E-02	(1,1) 0.122424500E-06 (1,2) 0.15369200E-05 (1,3) 0.125545400E-05 (1,4) 0.26719200E-05 (1,5) 0.96315400E-02 (1,6) 0.78470800E-01	(1,1) 0.51065100E-04 (1,2) 0.66888800E-04 (1,3) 0.26719200E-03 (1,4) 0.11223000E-02 (1,5) 0.38893200E-01 (1,6) 0.51312400E-01	(1,1) 0.22915300E-04 (1,2) 0.153100E-04 (1,3) 0.96315400E-02 (1,4) 0.38893200E-01 (1,5) 0.13657200E-01 (1,6) 0.21526100E-01	(1,1) 0.2184580E-02 (1,2) 0.3483000E-02 (1,3) 0.78470800E-01 (1,4) 0.51312400E-01 (1,5) 0.21526100E-01 (1,6) 0.82627600E-01					
20	(1,1) 0.12910000E-05 (1,2)-0.320213300E-05 (1,3)-0.23569200E-05 (1,4) 0.39544500E-02 (1,5) 0.10665900E-02 (1,6) 0.46393600E-00	(1,1) 0.12910000E-05 (1,2) 0.10919390E-06 (1,3) 0.11541100E-06 (1,4) 0.82512800E-02 (1,5) 0.10180900E-02 (1,6) 0.28948700E-01	(1,1) 0.11680400E-06 (1,2) 0.27558600E-06 (1,3) 0.50952000E-05 (1,4) 0.35569700E-03 (1,5) 0.91546500E-02 (1,6) 0.20466100E-02	(1,1) 0.12272700E-08 (1,2) 0.71394900E-08 (1,3) 0.85848400E-07 (1,4) 0.11541100E-07 (1,5) 0.48992500E-02 (1,6) 0.15590400E-03	(1,1) 0.13517400E-05 (1,2) -0.76601700E-07 (1,3) 0.11541100E-06 (1,4) 0.82512800E-02 (1,5) 0.10180900E-02 (1,6) 0.44584200E-01	(1,1) 0.13517400E-05 (1,2) 0.76601700E-07 (1,3) 0.11541100E-06 (1,4) 0.82512800E-02 (1,5) 0.10180900E-02 (1,6) 0.44584200E-01	(1,1) 0.21708500E-04 (1,2) 0.92461500E-03 (1,3) 0.20461500E-02 (1,4) 0.46393600E-00 (1,5) 0.12872399E-00 (1,6) 0.29152000E-01					
21	(1,1) 0.27585800E-07 (1,2)-0.122727100E-08 (1,3)-0.10919390E-06 (1,4) 0.13517400E-05 (1,5) 0.21708500E-04 (1,6) -0.11002600E-04	(1,1) 0.12476100E-07 (1,2)-0.65732400E-07 (1,3)-0.29667300E-06 (1,4) 0.74887700E-04 (1,5) 0.78603300E-03 (1,6) -0.19093900E-03	(1,1) 0.122727100E-08 (1,2) 0.71394900E-08 (1,3) 0.446180600E-07 (1,4) 0.11281200E-06 (1,5) 0.71715800E-03 (1,6) 0.14508700E-04	(1,1) 0.63732400E-07 (1,2) 0.10153690E-09 (1,3) 0.46180600E-07 (1,4) 0.11281200E-06 (1,5) 0.71715800E-03 (1,6) 0.73451600E-03	(1,1) 0.29667300E-06 (1,2) 0.12812000E-06 (1,3) 0.98502000E-07 (1,4) 0.12562500E-03 (1,5) 0.30296200E-02 (1,6) 0.13822400E-01	(1,1) 0.48679100E-04 (1,2) 0.12812000E-06 (1,3) 0.46180600E-06 (1,4) 0.12562500E-03 (1,5) 0.30296200E-02 (1,6) 0.16394200E-01	(1,1) 0.78603300E-03 (1,2) 0.71715800E-03 (1,3) 0.86443400E-02 (1,4) 0.90296200E-00 (1,5) 0.70002100E-00 (1,6) 0.15593699E-00					
22	(1,1) 0.11001900E-05 (1,2) -0.86261300E-05 (1,3) 0.14791800E-05 (1,4) 0.14791800E-05 (1,5) 0.16680500E-03 (1,6) 0.15610-0.36024400E-01	(1,1) 0.13670400E-03 (1,2) 0.14208700E-04 (1,3) 0.73451600E-03 (1,4) 0.16394200E-01 (1,5) 0.14054700E-00 (1,6) 0.26120700E-00	(1,1) 0.12476100E-07 (1,2) -0.65732400E-07 (1,3) -0.29667300E-06 (1,4) 0.74887700E-05 (1,5) 0.21708500E-03 (1,6) -0.11002600E-03	(1,1) 0.86925700E-06 (1,2) 0.11001900E-05 (1,3) 0.33707800E-06 (1,4) 0.12019300E-05 (1,5) 0.38862800E-03 (1,6) -0.13670400E-03	(1,1) 0.41879100E-07 (1,2) 0.649672000E-08 (1,3) 0.124234100E-06 (1,4) 0.17791800E-05 (1,5) 0.14933800E-02 (1,6) 0.131817100E-04	(1,1) 0.14622300E-06 (1,2) 0.10081600E-07 (1,3) 0.14749700E-06 (1,4) 0.12920600E-04 (1,5) 0.10989800E-02 (1,6) 0.14612400E-01	(1,1) 0.19252700E-05 (1,2) 0.13182500E-06 (1,3) 0.12920600E-06 (1,4) 0.16688500E-03 (1,5) 0.10989800E-02 (1,6) 0.96383900E-01					
23	(1,1) 0.12632500E-04 (1,2) 0.86875000E-04 (1,3) 0.16394200E-04 (1,4) 0.16394200E-04 (1,5) 0.14612400E-01 (1,6) 0.67552700E-01	(1,1) 0.16913600E-03 (1,2) 0.11491799E-04 (1,3) 0.81986500E-02 (1,4) 0.14612400E-01 (1,5) 0.96383900E-01 (1,6) 0.26120700E-00	(1,1) 0.22689700E-07 (1,2) -0.15211000E-08 (1,3) 0.14622300E-06 (1,4) 0.19252700E-05 (1,5) 0.12692500E-04 (1,6) 0.16913600E-03	(1,1) 0.15211000E-08 (1,2) 0.10081600E-09 (1,3) 0.10081600E-07 (1,4) 0.1182500E-06 (1,5) 0.86875000E-04 (1,6) 0.11491799E-04	(1,1) 0.14622300E-06 (1,2) 0.10081600E-07 (1,3) 0.14749700E-06 (1,4) 0.12920600E-04 (1,5) 0.84351200E-02 (1,6) 0.91986500E-02	(1,1) 0.14622300E-06 (1,2) 0.19252700E-05 (1,3) 0.12920600E-06 (1,4) 0.16688500E-03 (1,5) 0.10989800E-02 (1,6) 0.14612400E-01	(1,1) 0.12632500E-04 (1,2) 0.86875000E-04 (1,3) 0.16394200E-04 (1,4) 0.16394200E-04 (1,5) 0.14612400E-01 (1,6) 0.67552700E-01					

a Locate the covariance matrix number on table A-V for a description of the events preceding T<sub>L</sub>.

TABLE A-VI. - Continued a  
Covariance Matrix

## Covariance Matrix

Number	(1,1) 0.12150860E-07 (1,2) -0.12001C99E-08 (1,3) 0.10424400E-06 (1,4) 0.13529100E-05 (1,5) -0.49333200E-03 (1,6) -0.67181700E-02	(1,1) 0.12001099E-08 (1,2) 0.11040200E-09 (1,3) -0.963121200E-06 (1,4) -0.12446400E-06 (1,5) 0.44607600E-04 (1,6) 0.63057000E-03	(1,1) -0.12001099E-08 (1,2) 0.11040200E-09 (1,3) -0.963121200E-06 (1,4) -0.12446400E-06 (1,5) 0.44607600E-04 (1,6) 0.63057000E-03
25	(1,1) 0.13529100E-05 (1,2) -0.12446400E-06 (1,3) 0.119500E-05 (1,4) 0.108542700E-04 (1,5) -0.39259400E-02 (1,6) -0.50281400E-01	(1,1) 0.13529100E-05 (1,2) -0.12446400E-06 (1,3) 0.119500E-05 (1,4) 0.108542700E-04 (1,5) -0.39259400E-02 (1,6) -0.50281400E-01	(1,1) 0.13529100E-05 (1,2) -0.12446400E-06 (1,3) 0.119500E-05 (1,4) 0.108542700E-04 (1,5) -0.39259400E-02 (1,6) -0.50281400E-01
26	(1,1) 0.49609400E-06 (1,2) -0.51331100E-07 (1,3) 0.28416100E-05 (1,4) 0.60947900E-04 (1,5) -0.53241800E-03 (1,6) -0.20869300E-02	(1,1) 0.49609400E-06 (1,2) -0.51331100E-07 (1,3) 0.28416100E-05 (1,4) 0.60947900E-04 (1,5) -0.53241800E-03 (1,6) -0.20869300E-02	(1,1) 0.49609400E-06 (1,2) -0.51331100E-07 (1,3) 0.28416100E-05 (1,4) 0.60947900E-04 (1,5) -0.53241800E-03 (1,6) -0.20869300E-02
27	(1,1) 0.95139900E-06 (1,2) -0.58948300E-07 (1,3) 0.14356200E-05 (1,4) 0.445322600E-05 (1,5) -0.7013400E-04 (1,6) -0.1161-0.35681400E-02	(1,1) 0.95139900E-06 (1,2) -0.58948300E-07 (1,3) 0.14356200E-05 (1,4) 0.445322600E-05 (1,5) -0.7013400E-04 (1,6) -0.1161-0.35681400E-02	(1,1) 0.95139900E-06 (1,2) -0.58948300E-07 (1,3) 0.14356200E-05 (1,4) 0.445322600E-05 (1,5) -0.7013400E-04 (1,6) -0.1161-0.35681400E-02
28	(1,1) 0.24761200E-07 (1,2) -0.43045000E-07 (1,3) 0.16778800E-08 (1,4) -0.19481700E-04 (1,5) -0.14778200F-05 (1,6) -0.12979100F-03	(1,1) 0.24761200E-07 (1,2) -0.43045000E-07 (1,3) 0.16778800E-08 (1,4) -0.19481700E-04 (1,5) -0.14778200F-05 (1,6) -0.12979100F-03	(1,1) 0.24761200E-07 (1,2) -0.43045000E-07 (1,3) 0.16778800E-08 (1,4) -0.19481700E-04 (1,5) -0.14778200F-05 (1,6) -0.12979100F-03
29	(1,1) 0.43045000E-07 (1,2) -0.23818200E-08 (1,3) 0.11193900E-09 (1,4) 0.244402300E-05 (1,5) 0.29836500E-02 (1,6) -0.35493200E-02	(1,1) 0.43045000E-07 (1,2) -0.23818200E-08 (1,3) 0.11193900E-09 (1,4) 0.244402300E-05 (1,5) 0.29836500E-02 (1,6) -0.35493200E-02	(1,1) 0.43045000E-07 (1,2) -0.23818200E-08 (1,3) 0.11193900E-09 (1,4) 0.244402300E-05 (1,5) 0.29836500E-02 (1,6) -0.35493200E-02

a) Locate the covariance matrix number on table A-V for a description of the events preceding T<sub>1</sub>.

TABLE A-VI. - Concluded<sup>a</sup>

## Covariance Matrix

Number	(1,1)	0.2277410CE_07	(1,2)-0.14470D00E_08	(1,3)	0.13370500E_06	(1,4)	0.18075600E_05	(1,5)-0.13730800E_04	(1,6)	0.11545200E_02	
31	(2,1)	-0.14470000E_08	C8 (2,2)	0.92578300E_06	(2,3)	-0.82514200E_06	(2,4)	-0.11567800E_06	(2,5)	0.8635500E_04	
	(3,1)	0.13370500E_06	(3,2)	-0.82514200E_06	(3,3)	0.17696400E_05	(3,4)	0.10277200E_04	(3,5)	-0.81412700E_02	
	(4,1)	0.18075600E_05	(4,2)	-0.11567800E_06	(4,3)	0.10277200E_04	(4,4)	0.14454800E_03	(4,5)	-0.10855600E_02	
	(5,1)	-C13730800E_04	(5,2)	0.8693500E_04	(5,3)	-0.51412700E_02	(5,4)	-0.10855600E_02	(5,5)	0.84559800E_00	
	(6,1)	0.11545200E_02	(6,2)	-0.97400300E_02	(6,3)	0.72505600E_01	(6,4)	0.12421200E_00	(6,5)	-0.17135400E_-02	
32	(1,1)	0.30785300E_07	(1,2)-0.40101500E_08	(1,3)	0.24627400E_05	(1,4)	0.48229400E_05	(1,5)	-0.13534200E_04	(1,6)	0.23004700E_03
	(2,1)	-0.40101500E_08	(2,2)	0.52469200E_09	(2,3)	-0.32314200E_06	(2,4)	-0.63130200E_06	(2,5)	0.17589800E_05	
	(3,1)	0.28627400E_05	(3,2)	-0.32314200E_06	(3,3)	0.31313100E_05	(3,4)	0.39468800E_03	(3,5)	-0.16046900E_02	
	(4,1)	0.48229400E_05	(4,2)	-0.63130200E_06	(4,3)	0.39468800E_03	(4,4)	0.756958200E_03	(4,5)	-0.21176800E_02	
	(5,1)	-0.13534200E_04	(5,2)	0.17589800E_05	(5,3)	-0.16046900E_02	(5,4)	-0.21176800E_02	(5,5)	0.60874400E_00	
	(6,1)	0.23004700E_03	(6,2)	-0.29464500E_04	(6,3)	0.11663300E_02	(6,4)	0.35665700E_01	(6,5)	-0.10101400E_00	

<sup>a</sup> Locate the covariance matrix number on table A-V for a description of the events preceding TII.

APPENDIX B  
TRANSLUNAR INJECTION MANEUVER PROCEDURES

## APPENDIX B

## TRANSLUNAR INJECTION MANEUVER PROCEDURES

Reference 5 describes a program which propagates a covariance matrix through powered-flight maneuvers. The following are the main inputs to the program:

1. An ephemeris of the maneuver containing time, position and velocity, thrust angles with respect to the local vertical and fuel used at 5-second intervals throughout the maneuver.
2. Initial covariance matrix of position and velocity.
3. Variances in scale factor error, platform misalignment and drift and accelerometer bias.

The ephemeris of the maneuver was generated by the Apollo Reference Mission Program (ARMP). The navigation uncertainties were taken from references 4 and 6.

The covariance matrices (appendix A) at TLI are in the local vertical system. They were rotated to the inertial system of the ephemeris by the following transformation (ref. 7).

$$\overset{'}{P}_o = C_o P_o C_o^T$$

Where:

$P_o$  is the state covariance matrix in the local vertical system.

$\overset{'}{P}_o$  is the covariance matrix in the inertial system of the ephemeris of the TLI maneuver.

$$C_o \text{ } 6 \times 6 = \begin{bmatrix} D_o & | & \bar{0} \\ \hline \bar{0} & | & D_o \end{bmatrix}$$

$\bar{0}$  is  $3 \times 3$  null matrix.

$$D_o = \begin{bmatrix} R_o & (R_o \times V_o) \times R_o & R_o \times V_o \\ \hline R_o & [(R_o \times V_o) \times R_o] & [R_o \times V_o] \end{bmatrix} \text{ } 3 \times 3$$

$R_o$  and  $V_o$  expressed in the inertial system at the start of the maneuver.

The covariance matrix at the end of TLI is based only upon dispersions in the estimated state (actual - estimated) at the start of TLI and dispersions in the navigation parameters. The engine uncertainties do not affect the onboard estimate since the accelerometers integrate the thrust acceleration during the maneuver and correct for non-nominal variations occurring in engine parameters.

This study assumes that the tailoff thrust profile is built into the guidance package, and that there is no deviation from nominal cutoff conditions if the navigation system is error free and perfect knowledge of the vehicle's position and velocity at the start of TLI is assumed. The S-IVB IU or CM estimate of position and velocity at the end of the TLI maneuver was assumed to be the desired vector.

Table B-I and table B-II present formats of the covariance matrices at the end of the TLI maneuver (table B-III) in the local vertical coordinate system defined at that time.

TABLE B-I.- FORMAT OF THE COVARIANCE MATRICES AT THE END OF THE TLI MANEUVER

Time of TLI, minutes after EPOI	Approximate time of vector update (if applicable) minutes after EPOI (a)	Navigation system considered and covariance matrix number					
		10		Ground and IU		Ground and CM <sup>b</sup>	
		No Drift	Drift	No Drift	Drift	No platform alignment	Platform alignment
72.6° Launch azimuth; +27.5° lunar declination							
131.0	90.	33	49	65	81	--	--
145.0	90.	34	50	66	82	--	--
218.5	180.	35	51	67	83	--	--
232.5	180.	36	52	68	84	--	--
72.6° Launch azimuth; -27.5° lunar declination							
86.0	50.	37	53	69	85	--	--
101.0	50.	38	54	70	86	--	--
173.0	136.	39	55	71	87	--	--
188.5	136.	40	56	72	88	--	--
260.5	228.	41	57	73	89	--	--
90° Launch azimuth; -27.5° lunar declination							
168.0	135.	42	58	74	90	113 <sup>b</sup>	116 <sup>b</sup>
176.0	135.	43	59	75	91	114 <sup>b</sup>	117 <sup>b</sup>
256.0	197.	44	60	76	92	115	118
108° Launch azimuth; -27.5° lunar declination							
85.0	55.	45	61	77	93	--	--
157.5	83.	46	62	78	94	--	--
172.5	147.	47	63	79	95	--	--
244.5	172.	48	64	80	96	--	--

<sup>a</sup>See table A-II for ground track profile.<sup>b</sup>The update was uplinked to the CM, but the values were those predicted by the ground navigation system to the start of TLI.

TABLE B-II.- FORMAT OF THE COVARIANCE MATRICES AT  
THE END OF THE TLI MANEUVER

Time of TLI, minutes after EPOI	Approximate time of vector update (if applicable) in minutes after EPOI (a)	Individual error sources of the ground and IU	Covariance matrix number
Anytime	Anytime <sup>b</sup>	IU scale factor and bias during TLI. Other IU navigation hardware and software perfect.	97
86.0	b86.	IU launch pad misalignment and drift to TLI. Other IU navigation hardware and software perfect.	98
101.0	b101.		99
173.0	b173.		100
188.5	b188.5		101
260.5	b260.5		102
72.6° Launch azimuth; -27.5° lunar declination			
86.0	--	IU estimate of position and velocity at the start of TLI in error due to S-IVB IU navigation errors during the launch and earth orbit phases. Perfect IU navigation during the TLI maneuver.	103
101.0	--		104
173.0	--		105
188.5	--		106
260.5	--		107
Launch azimuth; -27.5° lunar declination			
86.0	50.	IU estimate of position and velocity at the start of TLI in error due to ground navigation error and IU earth orbit navigation error from the time of the update to the start of TLI. Perfect IU navigation during the TLI maneuver.	108
101.0	50.		109
173.0	136.		110
188.5	136.		111
260.5	228.		112

<sup>a</sup>See table A-II for ground track profile.

<sup>b</sup>Perfect update uplinked to S-IVB.

TABLE B-III.- COVARIANCE MATRICES AT THE END OF THE TLI MANEUVER  
Covariance Matrix

Number	LAT3 MATRIX																																				
33	<p><b>LAT3 MATRIX</b></p> <table border="1"> <tr><td>0.56388663E C7</td><td>-0.33622185E CB</td><td>-0.24691031E 05</td><td>0.41764464E 05</td><td>-0.98082423E 04</td><td>-0.13684825E 02</td></tr> <tr><td>-0.23623784E C8</td><td>0.34353404E C9</td><td>0.16793200E C5</td><td>-0.38877595E 06</td><td>-0.71762414E 05</td><td>-0.54779744E 01</td></tr> <tr><td>-0.24651750E C5</td><td>0.16753200E C5</td><td>2.12297656E C7</td><td>-0.20195889E 03</td><td>0.42562292E 02</td><td>0.30069039E 04</td></tr> <tr><td>0.41164466E C5</td><td>-0.38871596E 06</td><td>-0.20195927E C3</td><td>0.46446150E 03</td><td>-0.8721120E 02</td><td>-0.85933805E -02</td></tr> <tr><td>-0.588CE2417E 04</td><td>0.71762416E 05</td><td>0.42561530E 02</td><td>-0.8722118E 02</td><td>0.18638923E 02</td><td>0.54516792E -02</td></tr> <tr><td>-0.13686035E C2</td><td>-0.54765225E 01</td><td>0.30069024E 04</td><td>-0.85964235E -02</td><td>0.54526329E -02</td><td>0.13920197E 02</td></tr> </table>	0.56388663E C7	-0.33622185E CB	-0.24691031E 05	0.41764464E 05	-0.98082423E 04	-0.13684825E 02	-0.23623784E C8	0.34353404E C9	0.16793200E C5	-0.38877595E 06	-0.71762414E 05	-0.54779744E 01	-0.24651750E C5	0.16753200E C5	2.12297656E C7	-0.20195889E 03	0.42562292E 02	0.30069039E 04	0.41164466E C5	-0.38871596E 06	-0.20195927E C3	0.46446150E 03	-0.8721120E 02	-0.85933805E -02	-0.588CE2417E 04	0.71762416E 05	0.42561530E 02	-0.8722118E 02	0.18638923E 02	0.54516792E -02	-0.13686035E C2	-0.54765225E 01	0.30069024E 04	-0.85964235E -02	0.54526329E -02	0.13920197E 02
0.56388663E C7	-0.33622185E CB	-0.24691031E 05	0.41764464E 05	-0.98082423E 04	-0.13684825E 02																																
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0.38202C284E C7	-0.21542382E 08	-0.30456039E 05	0.26676452E 05	-0.76238446E 04	0.18277207E 01																																
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35	<p><b>LAT3 MATRIX</b></p> <table border="1"> <tr><td>0.324466835E C7</td><td>-0.5007078495E 08</td><td>-0.322436883E 05</td><td>0.60971621E 05</td><td>-0.97059953E 04</td><td>-0.85272674E 01</td></tr> <tr><td>-0.50C78498E C8</td><td>0.15552636E 10</td><td>0.81118970E 06</td><td>-0.18161866E 07</td><td>0.23594723E 06</td><td>-0.91250721E 02</td></tr> <tr><td>-0.32446637E C5</td><td>0.81115400E 06</td><td>0.12372231E C7</td><td>-0.95404102E 03</td><td>0.12850013E 03</td><td>0.30078395E 04</td></tr> <tr><td>-0.60971622E C5</td><td>-0.18161866E 07</td><td>-0.55404767E 03</td><td>0.21332688E 04</td><td>-0.27916256E 03</td><td>0.91639757E -01</td></tr> <tr><td>-0.97C59840E 04</td><td>0.23554123E 06</td><td>0.128494673E 03</td><td>-0.27916288E 03</td><td>0.38795770E 02</td><td>-0.90577006E -02</td></tr> <tr><td>-0.85272535E C1</td><td>-0.91234375E 02</td><td>0.30C78470E 04</td><td>0.91629028E -01</td><td>-0.90475032E -02</td><td>0.13910076E 02</td></tr> </table>	0.324466835E C7	-0.5007078495E 08	-0.322436883E 05	0.60971621E 05	-0.97059953E 04	-0.85272674E 01	-0.50C78498E C8	0.15552636E 10	0.81118970E 06	-0.18161866E 07	0.23594723E 06	-0.91250721E 02	-0.32446637E C5	0.81115400E 06	0.12372231E C7	-0.95404102E 03	0.12850013E 03	0.30078395E 04	-0.60971622E C5	-0.18161866E 07	-0.55404767E 03	0.21332688E 04	-0.27916256E 03	0.91639757E -01	-0.97C59840E 04	0.23554123E 06	0.128494673E 03	-0.27916288E 03	0.38795770E 02	-0.90577006E -02	-0.85272535E C1	-0.91234375E 02	0.30C78470E 04	0.91629028E -01	-0.90475032E -02	0.13910076E 02
0.324466835E C7	-0.5007078495E 08	-0.322436883E 05	0.60971621E 05	-0.97059953E 04	-0.85272674E 01																																
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36	<p><b>LAT3 MATRIX</b></p> <table border="1"> <tr><td>0.234466855E C7</td><td>-0.25613246E 08</td><td>-0.20412141E J5</td><td>0.42079391E C5</td><td>-0.67964223E 04</td><td>0.32774734E C1</td></tr> <tr><td>-0.351327E C8</td><td>0.20741666E 10</td><td>0.11370853E L7</td><td>-0.23706065E 07</td><td>0.2823022E 06</td><td>-0.19137836E C3</td></tr> <tr><td>-0.30466281E C5</td><td>0.113171760E 07</td><td>0.23841557E 07</td><td>-0.12958867E 04</td><td>0.16690820E 03</td><td>0.12836533E 04</td></tr> <tr><td>0.42C79401E C5</td><td>-0.23106666E C7</td><td>-0.12958843E 04</td><td>0.272292C9E C4</td><td>-0.32505829E 03</td><td>0.21411985E 00</td></tr> <tr><td>-0.67664312E C4</td><td>0.2823C23E 06</td><td>0.16530699E 03</td><td>-0.32505826E C3</td><td>0.4103257E 02</td><td>-0.33889636E -01</td></tr> <tr><td>0.3271444E 01</td><td>-0.19138281E C3</td><td>0.12834523E 04</td><td>0.214096C7t 00</td><td>-0.33878326E -01</td><td>0.1222721E C2</td></tr> </table>	0.234466855E C7	-0.25613246E 08	-0.20412141E J5	0.42079391E C5	-0.67964223E 04	0.32774734E C1	-0.351327E C8	0.20741666E 10	0.11370853E L7	-0.23706065E 07	0.2823022E 06	-0.19137836E C3	-0.30466281E C5	0.113171760E 07	0.23841557E 07	-0.12958867E 04	0.16690820E 03	0.12836533E 04	0.42C79401E C5	-0.23106666E C7	-0.12958843E 04	0.272292C9E C4	-0.32505829E 03	0.21411985E 00	-0.67664312E C4	0.2823C23E 06	0.16530699E 03	-0.32505826E C3	0.4103257E 02	-0.33889636E -01	0.3271444E 01	-0.19138281E C3	0.12834523E 04	0.214096C7t 00	-0.33878326E -01	0.1222721E C2
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0.226674747E C7	0.69529564E 07	-0.24392359E 03	-0.56260544E 04	-0.20889525E 04	-0.11251389E 02																																
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-0.20889521E C4	0.19408145C 04	0.27284602E 01	-0.50460610E 01	0.26478137E -03	0.24478137E -03																																
-0.11251679E 02	-0.54191406E 02	0.29566839E 04	0.45259476E -01	0.24494529F -03	0.1410920E 02																																
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-0.17234643RF 07	0.12277C4E 09	0.54430670E 05	-0.15622736E 06	0.1228127E 05	-0.21344024E 02																																
-0.11401156E 05	0.56431250E 05	-0.65552978E 07	-0.65552978E 02	0.17609474E 02	0.13407039E 04																																
0.38812450F 04	-0.1522736E 06	-0.65552139E 07	0.21126556E 03	-0.16805430E 02	0.22547185E -01																																
-0.22508512E 04	0.1283124E 05	0.17608822E 02	-0.168954629E 02	0.40426783E 01	-0.90993643E -02																																
-0.6471867RF 00	-0.21344024E 02	0.34677047C 04	0.22546768E -01	-0.49941196E -02	0.12206491F 02																																

a Locate the covariance matrix number on either table B-I or B-II  
for a description of the events preceding TLI.

TABLE B-III. - Continued a

## Covariance Matrix

Number	LAT3 MATRIX	Covariance Matrix
39	$\begin{pmatrix} 0.422062723E & 0.7 \\ 0.1334794F & 0.8 \\ 0.60668750E & 0.6 \\ -0.20476351E & 0.5 \\ -0.15763031E & 0.2 \end{pmatrix}$	$\begin{pmatrix} 0.60679453E & 0.6 \\ 0.39181710E & 0.6 \\ 0.96566081E & 0.6 \\ -0.45879784F & 0.3 \\ -0.7108665E & 0.2 \\ -0.10190755E & 0.1 \\ -0.1295449E & 0.2 \end{pmatrix}$
40	$\begin{pmatrix} 0.49400881E & 0.7 \\ 0.35020312E & 0.4 \\ -0.62974043F & 0.4 \\ -0.24830134E & 0.4 \\ -0.72465516F & 0.1 \end{pmatrix}$	$\begin{pmatrix} 0.96469052E & 0.7 \\ 0.41090016F & 0.6 \\ 0.50042039E & 0.3 \\ 0.13063115E & 0.4 \\ 0.55653119E & 0.2 \\ 0.12801896E & 0.2 \\ 0.12801896E & 0.1 \\ -0.18389702E & 0.1 \end{pmatrix}$
41	$\begin{pmatrix} 0.60016521E & 0.7 \\ 0.61322831E & 0.8 \\ 0.262239875E & 0.5 \\ 0.515F29581F & 0.5 \\ 0.548310748F & 0.3 \\ -0.232805667E & 0.2 \end{pmatrix}$	$\begin{pmatrix} 0.26259053E & 0.5 \\ 0.14482634F & 0.7 \\ 0.97285623E & 0.6 \\ 0.16468280CE & 0.7 \\ -0.3447944F & 0.7 \\ 0.27196408E & 0.6 \\ 0.45757912E & 0.3 \end{pmatrix}$
42	$\begin{pmatrix} 0.91155109F & 0.7 \\ 0.25714000E & 0.6 \\ 0.47684662E & 0.4 \\ -0.75719108E & 0.4 \\ -0.19628985E & 0.4 \\ -0.94245911E & 0.1 \end{pmatrix}$	$\begin{pmatrix} 0.91155120E & 0.7 \\ 0.35713481E & 0.6 \\ 0.38266952E & 0.6 \\ 0.40918879E & 0.3 \\ 0.3792507E & 0.2 \\ -0.13707429E & 0.3 \end{pmatrix}$
43	$\begin{pmatrix} 0.40275301E & 0.7 \\ 0.12653053E & 0.8 \\ 0.3589150CE & 0.6 \\ 0.85676673F & 0.5 \\ -0.29590846E & 0.4 \\ -0.14091064F & 0.2 \end{pmatrix}$	$\begin{pmatrix} 0.68078125E & 0.2 \\ 0.35891539E & 0.6 \\ 0.42565723E & 0.7 \\ 0.47565711F & 0.3 \\ 0.43620875E & 0.2 \\ 0.30136200E & 0.4 \\ 0.207144639E & 0.3 \\ 0.2901172F & 0.3 \end{pmatrix}$
44	$\begin{pmatrix} 0.37709468E & 0.8 \\ 0.1931775CE & 0.5 \\ -0.40372194E & 0.5 \\ 0.29020785E & 0.2 \\ -0.16488461E & 0.2 \end{pmatrix}$	$\begin{pmatrix} 0.13242588E & 0.7 \\ 0.25743074E & 1.0 \\ 0.1324260CE & 0.7 \\ -0.207144639E & 0.7 \\ 0.2585552CEE & 0.6 \\ 0.39000000F & 0.3 \end{pmatrix}$
	LAT3 MATRIX	$\begin{pmatrix} 0.24053955E & 0.2 \\ 0.2585211E & 0.6 \\ 0.13163232E & 0.3 \\ 0.30284401E & 0.3 \\ 0.29872302E & 0.2 \\ -0.37829399E & 0.1 \\ 0.14490921E & 0.2 \end{pmatrix}$
	LAT3 MATRIX	$\begin{pmatrix} 0.13530648E & 0.0 \\ 0.13530648E & 0.0 \end{pmatrix}$

a Locate the covariance matrix number on either table B-1 or B-II  
for a description of the events preceding TLL.

TABLE B-III. - Continued <sup>a</sup>  
Covariance Matrix

Number	LAT <sub>3</sub> MATRIX	LAT <sub>2</sub> MATRIX	LAT <sub>3</sub> MATRIX	LAT <sub>2</sub> MATRIX	LAT <sub>3</sub> MATRIX	LAT <sub>2</sub> MATRIX	
45	0.21375725E 07 0.67397856F 07 0.12268474E 09 0.52742000E 05 0.19503166E 04 0.10678755E 02	0.46728906E 03 0.52547249E 04 0.52743792E 05 0.65863770E 02 0.52744236E 01 0.52744236E 01	0.19503166E 04 0.19608183E 04 0.19743792E 01 0.19744229E 01 0.19744229E 01 0.19744229E 01	0.19503166E 04 0.19608183E 04 0.19743792E 01 0.19744229E 01 0.19744229E 01 0.19744229E 01	0.10678755E 02 0.54680088E 02 0.28818344E 04 0.44078878E -01 0.54231286E -03 0.14407586E 02	0.10678755E 02 0.54680088E 02 0.28818344E 04 0.44078878E -01 0.54231286E -03 0.14407586E 02	0.10678755E 02 0.54680088E 02 0.28818344E 04 0.44078878E -01 0.54231286E -03 0.14407586E 02
46	0.61452091E 07 0.70200110E 09 0.39082805E 06 0.89104114E 04 0.23428017E 04	0.29982422E 06 0.76850224E 06 0.43612254E 06 0.91209532E 05 0.12784792E 03	0.77683536E 06 0.43612254E 06 0.87405612E 03 0.92027266E 02 0.12407100E 00	0.89104114E 06 0.87405612E 03 0.92027266E 02 0.11174820E 02 0.27691632E -01	0.89104114E 06 0.87405612E 03 0.92027266E 02 0.11174820E 02 0.14514838E 02	0.43161621E 01 0.12784792E 03 0.58525225E 03 0.12407100E 00 0.27691632E -01	0.43161621E 01 0.12784792E 03 0.58525225E 03 0.12407100E 00 0.27691632E -01
47	0.41046675E 07 0.19992087E 08 0.61737500E 04 0.19388842E 05 0.22629727E 04	0.18992049E 08 0.79875907E 09 0.89270641E 06 0.45914035E 06 0.62305226E 05	0.61737382E 06 0.39977652E 06 0.89270641E 06 0.454914035E 03 0.32769655E 02	0.19388842E 05 0.76825516E 06 0.89104114E 06 0.10737797E 04 0.76781627E 02	0.19388842E 05 0.76825516E 06 0.89104114E 06 0.10737797E 04 0.90902578E 01	0.41046675E 07 0.19992087E 08 0.61737500E 04 0.19388842E 05 0.22629727E 04	0.41046675E 07 0.19992087E 08 0.61737500E 04 0.19388842E 05 0.22629727E 04
48	0.81090920E 07 0.83623287E 03 0.11290001E 01	0.24672192E 10 0.13262620E 07 0.34971572E 05	0.28127410E 07 0.15119101E 04 0.15119101E 04	0.28127410E 07 0.15119101E 04 0.32217053E 04	0.81090920E 07 0.83623287E 03 0.11290001E 01	0.24672192E 10 0.13262620E 07 0.34971572E 05	0.24672192E 10 0.13262620E 07 0.34971572E 05
49	0.58289150E 07 0.13533105E 05 0.17757168E 02	0.39571572E 06 0.27860793E 06 0.23257812E 02	0.20506879E 03 0.15193621E 03 0.54305674E 03	0.20506879E 03 0.15193621E 03 0.54305674E 03	0.20506879E 03 0.15193621E 03 0.54305674E 03	0.39571572E 06 0.27860793E 06 0.23257812E 02	0.39571572E 06 0.27860793E 06 0.23257812E 02
50	0.65337254E 07 0.32715432E 08 0.31374891E 05	0.34286757E 08 0.54631566E 09 0.31422295E 06	0.255440761E 05 0.16549555E 06 0.35047571E 07	0.255440761E 05 0.16549555E 06 0.35047571E 07	0.255440761E 05 0.16549555E 06 0.35047571E 07	0.31375219E 05 0.31422295E 06 0.35047571E 07	0.31375219E 05 0.31422295E 06 0.35047571E 07

<sup>a</sup> Locate the covariance matrix number on either table B-I or B-II for a description of the events preceding TLI.

TABLE B-III.- Continued <sup>a</sup>

## Covariance Matrix

**a** Locate the covariance matrix number on either table B-1 or B-11 for a description of the events preceding TLI.

TABLE B-III. - Continued<sup>a</sup>

## Covariance Matrix

Number	LAT <sub>3</sub> MATRIX	LAT <sub>4</sub> MATRIX	LAT <sub>5</sub> MATRIX	LAT <sub>6</sub> MATRIX		
57	0.1515828F 08 0.5770331CE 08 0.23298625E 05 0.22701992E 04 -0.14639619E 05 -0.14639619E 05	0.23298625E 07 0.28025386CE 07 0.35311881F 06 0.79790821F 06 0.64391112E 05 0.27657371F 07	0.35147813E 04 0.19661488E 05 -0.41424125E 07 -0.41424125E 07 0.15020569E 02 0.15020569E 02	0.19661488E 05 -0.27657371F 07 0.12227582E 03 0.12227582E 03 0.19591296E 02 0.19591296E 02	-0.14639619E 05 -0.14639619E 05 0.57365192E 02 0.57365192E 02 0.31327772E 00 0.31327772E 00	
58	0.5770330F 08 0.1438644CE 07 0.2270183F 04 -0.32643217F 07 -0.16997956E 04 0.27659874F 06	0.14216723F 02 0.5782812E 03 0.67197542E 05 0.644412231F 00 0.644412231F 00	0.14216723F 07 0.25412110E 06 0.41246125E 06 0.41246125E 06 0.29060199D 07	0.14216723F 07 0.16997956E 04 0.3815559E 04 0.3815559E 04 0.10165259E 03	-0.27659874F 06 0.16997956E 04 0.32643217F 03 0.12232582E 03 0.10393719E 03	-0.52780872E 06 0.67192549E 03 0.44417191E 03 0.31327772E 00 0.4754095DF 03
59	0.19661489F 05 0.64391104E 05 0.8284324E 04 0.15474975F 07	0.11456871E 08 0.75446718E 09 0.35434090CE 06 0.17176114F 05	0.128466875E 04 0.254461976E 06 0.55343703E 07 0.43126563E 03	0.171776118E 05 0.86528463E 06 0.43126563E 03 0.12322932E 04	0.171776118E 04 0.65158119E 05 0.19991089E 02 0.12867580E 03	-0.15474975F 04 0.10393719E 03 0.12232582E 03 0.17909603E 00
60	0.28951651E 06 0.21821899F 07	0.11456871E 08 0.16409554E 03	0.128466875E 05 0.23263543E 02	0.171776118E 05 0.12867580E 03 0.21941605E 02 0.13265575E 00	-0.21825195E 02 0.64409192E 03 0.32363445E 05 0.10757256E 00	0.20709964E 03
61	0.12806081E 08 0.30846637F 02	0.11456871E 08 0.15177820E 08	0.164466937E 05 0.226664152E 05	0.164466937E 05 0.226664152E 05	0.14641262E 05 0.14641262E 05	-0.30841797E 02
62	0.64602544F 07 0.92031250F 02 0.17179557F 04 0.35722129F 04 0.12485833F 02	0.64661255E 07 0.12277676E 09 0.51714316F 05 0.14079079E 06 0.67174975F 02	0.91344250E 02 0.29903250E 07 0.15439727E 04 0.39134754E 04 0.22161188F 03	0.17179557E 04 0.14709071F 06 0.184546227F 07 0.14079079E 02 0.67174975F 02	0.35722132E 04 0.1851134E 04 0.952222118E 02 0.41226997E 02 0.52063000E 01	-0.4478253E 03 0.64476683E 05 0.3480777E 00 0.3044576E 00 0.4604679E 03

<sup>a</sup> Locate the covariance matrix number on either table B-1 or B-11 for a description of the events preceding TLI.

TABLE B-III.- Continued  
Covariance Matrix

Number	LAT3 MATRIX	LAT3 VARIETY	LAT3 MATRIX	LAT3 VARIETY	LAT3 MATRIX
63	$\begin{pmatrix} 0 & 0.79452361F & 0.7 \\ 0 & 0.79011924F & 0.9 \\ 0 & 0.38505465F & 0.9 \end{pmatrix}$ $\begin{pmatrix} 0 & 0.48748455F & 0.8 \\ 0 & 0.48722333F & 0.8 \\ 0 & 0.02474285F & 0.8 \end{pmatrix}$ $\begin{pmatrix} 0 & 0.80269167F & 0.8 \\ 0 & 0.65700920F & 0.8 \\ 0 & 0.27373307F & 0.8 \end{pmatrix}$	$\begin{pmatrix} 0.48748425E & 0.8 \\ 0.38505433E & 0.8 \\ 0.20480871F & 0.8 \end{pmatrix}$ $\begin{pmatrix} 0.48259321E & 0.7 \\ 0.46030337E & 0.7 \\ 0.16142205E & 0.7 \end{pmatrix}$ $\begin{pmatrix} 0.15159204E & 0 \\ 0.21679036E & 0 \\ 0.21679036E & 0 \end{pmatrix}$	$\begin{pmatrix} 0.92473789E & 0.4 \\ 0.92918876F & 0.6 \\ 0.16142822E & 0.2 \end{pmatrix}$ $\begin{pmatrix} 0.12973100F & 0.4 \\ 0.118552783E & 0.3 \\ 0.42087318E & 0.2 \end{pmatrix}$ $\begin{pmatrix} 0.26668176E & 0.3 \\ 0.20522662E & 0.3 \\ 0.20522662E & 0.3 \end{pmatrix}$	$\begin{pmatrix} 0.89269093E & 0.4 \\ 0.65700970E & 0.5 \\ 0.15176392E & 0.5 \end{pmatrix}$ $\begin{pmatrix} 0.13158089E & 0.5 \\ 0.15176392E & 0.5 \\ 0.15176392E & 0.5 \end{pmatrix}$	$\begin{pmatrix} -0.222729858E & 0.2 \\ -0.21104834E & 0.3 \\ -0.51156725E & 0.5 \end{pmatrix}$ $\begin{pmatrix} 0.31854057E & 0.0 \\ 0.29511452E & 0.0 \\ 0.420668176E & 0.3 \end{pmatrix}$
64	$\begin{pmatrix} 0 & 0.71888782F & 0.7 \\ 0 & 0.24670097E & 1.0 \\ 0 & 0.28929380F & 0.7 \end{pmatrix}$ $\begin{pmatrix} 0 & 0.15052535E & 0.4 \\ 0 & 0.49293505F & 0.5 \\ 0 & 0.14212618E & 0.5 \end{pmatrix}$ $\begin{pmatrix} 0 & 0.19803227F & 0.2 \\ 0 & 0.41104249E & 0.2 \\ 0 & 0.57156726F & 0.5 \end{pmatrix}$	$\begin{pmatrix} 0.11471562E & 0.4 \\ 0.13241298E & 0.7 \\ 0.15220466E & 0.4 \end{pmatrix}$ $\begin{pmatrix} 0.16503201F & 0.4 \\ 0.1854621F & 0.3 \\ 0.42087318E & 0.3 \end{pmatrix}$ $\begin{pmatrix} 0.31857300E & 0.0 \\ 0.31857300E & 0.0 \\ 0.31857300E & 0.0 \end{pmatrix}$	$\begin{pmatrix} 0.49203939E & 0.5 \\ 0.28904422E & 0.7 \\ 0.32272625E & 0.1 \end{pmatrix}$ $\begin{pmatrix} 0.15052535E & 0.4 \\ 0.15220466E & 0.4 \\ 0.20522662E & 0.4 \end{pmatrix}$ $\begin{pmatrix} 0.31857300E & 0.0 \\ 0.31857300E & 0.0 \\ 0.31857300E & 0.0 \end{pmatrix}$	$\begin{pmatrix} 0.14212618E & 0.5 \\ 0.20522662E & 0.5 \\ 0.20522662E & 0.5 \end{pmatrix}$ $\begin{pmatrix} 0.19803227F & 0.2 \\ 0.41104249E & 0.2 \\ 0.57156726F & 0.5 \end{pmatrix}$	$\begin{pmatrix} -0.13812500E & 0.2 \\ -0.21701706E & 0.6 \\ -0.51156725E & 0.5 \end{pmatrix}$ $\begin{pmatrix} 0.31854057E & 0.0 \\ 0.29511452E & 0.0 \\ 0.420668176E & 0.3 \end{pmatrix}$
65	$\begin{pmatrix} 0 & 0.14257175E & 0.7 \\ 0 & 0.420668175E & 0.7 \\ 0 & 0.15151111E & 0.4 \end{pmatrix}$ $\begin{pmatrix} 0 & 0.45427337E & 0.4 \\ 0 & 0.57253261E & 0.4 \\ 0 & 0.14257175E & 0.4 \end{pmatrix}$	$\begin{pmatrix} 0.14257175E & 0.7 \\ 0.420668175E & 0.7 \\ 0.15151111E & 0.4 \end{pmatrix}$ $\begin{pmatrix} 0.45427337E & 0.4 \\ 0.57253261E & 0.4 \\ 0.14257175E & 0.4 \end{pmatrix}$	$\begin{pmatrix} 0.420668175E & 0.7 \\ 0.15151111E & 0.4 \\ 0.14257175E & 0.4 \end{pmatrix}$ $\begin{pmatrix} 0.45427337E & 0.4 \\ 0.57253261E & 0.4 \\ 0.14257175E & 0.4 \end{pmatrix}$	$\begin{pmatrix} 0.14257175E & 0.7 \\ 0.420668175E & 0.7 \\ 0.15151111E & 0.4 \end{pmatrix}$ $\begin{pmatrix} 0.45427337E & 0.4 \\ 0.57253261E & 0.4 \\ 0.14257175E & 0.4 \end{pmatrix}$	$\begin{pmatrix} -0.14217661E & 0.2 \\ -0.21104834E & 0.3 \\ -0.51156725E & 0.5 \end{pmatrix}$ $\begin{pmatrix} 0.31854057E & 0.0 \\ 0.29511452E & 0.0 \\ 0.420668176E & 0.3 \end{pmatrix}$
66	$\begin{pmatrix} 0 & 0.41427123E & 0.7 \\ 0 & 0.37061564E & 0.6 \\ 0 & 0.40857656E & 0.4 \end{pmatrix}$ $\begin{pmatrix} 0 & 0.16477074E & 0.4 \\ 0 & 0.19064420E & 0.4 \\ 0 & 0.37573378E & 0.4 \end{pmatrix}$	$\begin{pmatrix} 0.27061562E & 0.7 \\ 0.40859323F & 0.6 \\ 0.38251051E & 0.4 \end{pmatrix}$ $\begin{pmatrix} 0.32838363E & 0.3 \\ 0.32453424E & 0.3 \\ 0.25572992E & 0.4 \end{pmatrix}$	$\begin{pmatrix} 0.27061562E & 0.7 \\ 0.40859323F & 0.6 \\ 0.32838363E & 0.3 \end{pmatrix}$ $\begin{pmatrix} 0.40857656E & 0.4 \\ 0.19064420E & 0.4 \\ 0.37573378E & 0.4 \end{pmatrix}$	$\begin{pmatrix} 0.16477074E & 0.4 \\ 0.19064420E & 0.4 \\ 0.37573378E & 0.4 \end{pmatrix}$ $\begin{pmatrix} 0.27061562E & 0.7 \\ 0.40859323F & 0.6 \\ 0.32838363E & 0.3 \end{pmatrix}$ $\begin{pmatrix} 0.40857656E & 0.4 \\ 0.19064420E & 0.4 \\ 0.37573378E & 0.4 \end{pmatrix}$	$\begin{pmatrix} -0.24655715CF & 0.2 \\ -0.21104834F & 0.3 \\ -0.51156725E & 0.5 \end{pmatrix}$ $\begin{pmatrix} 0.31854057E & 0.0 \\ 0.29511452E & 0.0 \\ 0.420668176E & 0.3 \end{pmatrix}$
67	$\begin{pmatrix} 0 & 0.27577377E & 0.7 \\ 0 & 0.37573378E & 0.4 \\ 0 & 0.21064420E & 0.4 \end{pmatrix}$	$\begin{pmatrix} 0.16477074E & 0.7 \\ 0.32453424E & 0.6 \\ 0.19064420E & 0.4 \end{pmatrix}$ $\begin{pmatrix} 0.19064420E & 0.4 \\ 0.37573378E & 0.4 \\ 0.21064420E & 0.4 \end{pmatrix}$	$\begin{pmatrix} 0.16477074E & 0.7 \\ 0.32453424E & 0.6 \\ 0.19064420E & 0.4 \end{pmatrix}$ $\begin{pmatrix} 0.27577377E & 0.4 \\ 0.37573378E & 0.4 \\ 0.21064420E & 0.4 \end{pmatrix}$	$\begin{pmatrix} 0.16477074E & 0.7 \\ 0.32453424E & 0.6 \\ 0.19064420E & 0.4 \end{pmatrix}$ $\begin{pmatrix} 0.27577377E & 0.4 \\ 0.37573378E & 0.4 \\ 0.21064420E & 0.4 \end{pmatrix}$	$\begin{pmatrix} -0.24655715CF & 0.2 \\ -0.21104834F & 0.3 \\ -0.51156725E & 0.5 \end{pmatrix}$ $\begin{pmatrix} 0.31854057E & 0.0 \\ 0.29511452E & 0.0 \\ 0.420668176E & 0.3 \end{pmatrix}$

TABLE B-III.- Continued <sup>a</sup>

Number	LATT. MATRIX
69	LATT. MATRIX 0.10207101 0.7 -0.17272620 0.7 -0.17272620 0.6 -0.7580461F 0.4 -0.1072000E 0.4 -0.56552417F 0.2 -0.5500204F 0.7 -0.17272620 0.7 -0.17272620 0.6 -0.7580461F 0.4 -0.1072000E 0.4 -0.56552417F 0.2 -0.17272620 0.7 -0.17272620 0.6 -0.7580461F 0.4 -0.1072000E 0.4 -0.56552417F 0.2 0.7580461F 0.6 -0.17272620 0.6 -0.17272620 0.5 -0.7465523E 0.3 -0.1065720E 0.3 -0.5500523E 0.1 -0.18719615 0.5 -0.17272620 0.5 -0.17272620 0.4 -0.1640315F 0.3 -0.3565229F 0.1 -0.3565229F 0.0 -0.863976 0.4 -0.17272620 0.4 -0.17272620 0.3 -0.4067320 0.2 -0.3565229F 0.1 -0.3565229F 0.0 -0.17272620 0.3 -0.17272620 0.2 -0.4067320 0.1 -0.3565229F 0.1 -0.3565229F 0.0
70	LATT. MATRIX 0.11226117F 0.7 -0.14722004F 0.7 -0.17571603F 0.6 -0.45166501AF 0.1 -0.10772147F 0.4 -0.53781298F 0.2 -0.14722004F 0.7 -0.17571603F 0.6 -0.45166501AF 0.1 -0.10772147F 0.4 -0.53781298F 0.2 0.17571603F 0.7 -0.14722004F 0.7 -0.17571603F 0.6 -0.45166501AF 0.1 -0.10772147F 0.4 -0.53781298F 0.2 -0.45166501AF 0.6 -0.17571603F 0.6 -0.17571603F 0.5 -0.5106599F 0.4 -0.2065621F 0.3 -0.50375326F 0.1 -0.17771157 0.5 -0.17571603F 0.5 -0.17571603F 0.4 -0.2065621F 0.3 -0.10414492F 0.1 -0.1672637F-0.1 -0.3701137E 0.4 -0.17571603F 0.4 -0.17571603F 0.3 -0.2065621F 0.2 -0.10414492F 0.1 -0.1672637F-0.1 -0.8787777F 0.3 -0.17571603F 0.3 -0.17571603F 0.2 -0.2065621F 0.1 -0.10414492F 0.1 -0.1672637F-0.1
71	LATT. MATRIX 0.55242514E 0.6 -0.2603100C 0.7 -0.77335600C 0.4 -0.1091444E 0.4 -0.974566792F 0.2 -0.55242514E 0.6 -0.2603100C 0.7 -0.77335600C 0.4 -0.1091444E 0.4 -0.974566792F 0.2 -0.2603100C 0.7 -0.55242514E 0.6 -0.6080160E 0.2 -0.2547609AF 0.1 -0.17824235F 0.1 0.77335600C 0.6 -0.55242514E 0.6 -0.6080160E 0.2 -0.2547609AF 0.1 -0.17824235F 0.1 -0.1091444E 0.5 -0.55242514E 0.5 -0.6080160E 0.1 -0.2547609AF 0.1 -0.10807754F 0.0 -0.3701137E 0.4 -0.55242514E 0.4 -0.6080160E 0.1 -0.2547609AF 0.1 -0.10807754F 0.0 -0.8787777F 0.3 -0.55242514E 0.3 -0.6080160E 0.1 -0.2547609AF 0.1 -0.10807754F 0.0
72	LATT. MATRIX 0.12617101 0.7 -0.11262605 0.6 -0.12617101 0.6 -0.15611497F 0.5 -0.244232127F 0.4 -0.456644352F 0.2 -0.15611497F 0.6 -0.12617101 0.6 -0.15611497F 0.5 -0.244232127F 0.4 -0.456644352F 0.2 0.12617101 0.7 -0.15611497F 0.6 -0.1465677F 0.4 -0.29757685F 0.5 -0.2547609AF 0.1 -0.17112053F 0.1 -0.16411437E 0.5 -0.15611497F 0.6 -0.1465677F 0.4 -0.29757685F 0.5 -0.2547609AF 0.1 -0.17112053F 0.1 -0.244232127F 0.4 -0.15611497F 0.5 -0.1465677F 0.3 -0.2023336F 0.3 -0.2023336F 0.0 -0.69120045 0.3 -0.15611497F 0.4 -0.1465677F 0.2 -0.4786110F 0.1 -0.4786110F 0.0 -0.13591515F 0.0 -0.35674351E 0.2 -0.15611497F 0.3 -0.1465677F 0.1 -0.1223415F 0.1 -0.1223415F 0.0
73	LATT. MATRIX 0.3116600F 0.6 -0.13267404F 0.7 -0.16570720F 0.6 -0.12617101 0.5 -0.244232127F 0.4 -0.456644352F 0.2 -0.2023336F 0.5 -0.13267404F 0.6 -0.12617101 0.5 -0.244232127F 0.4 -0.456644352F 0.2 0.15611497F 0.6 -0.13267404F 0.6 -0.12617101 0.5 -0.244232127F 0.4 -0.456644352F 0.2 -0.50220035 0.5 -0.13267404F 0.5 -0.12617101 0.4 -0.15711458F 0.3 -0.1792041F 0.1 -0.8736397E-0.1 -0.69120045 0.4 -0.13267404F 0.4 -0.12617101 0.3 -0.15711458F 0.2 -0.1792041F 0.1 -0.8736397E-0.1 -0.35674351E 0.3 -0.13267404F 0.3 -0.12617101 0.2 -0.15711458F 0.1 -0.1792041F 0.1 -0.8736397E-0.1
74	LATT. MATRIX 0.6112000F 0.6 -0.13267404F 0.7 -0.11042620 0.6 -0.57732641E 0.4 -0.05231675E 0.3 -0.2023336F 0.2 -0.2023336F 0.7 -0.13267404F 0.6 -0.11042620 0.5 -0.57732641E 0.4 -0.05231675E 0.3 -0.2023336F 0.2 0.13267404F 0.6 -0.13267404F 0.6 -0.11042620 0.5 -0.57732641E 0.4 -0.05231675E 0.3 -0.2023336F 0.2 -0.57732641E 0.5 -0.13267404F 0.5 -0.11042620 0.4 -0.1065720E 0.3 -0.1646460CE 0.1 -0.17046115F 0.1 -0.57732641E 0.4 -0.13267404F 0.4 -0.11042620 0.3 -0.1065720E 0.2 -0.1646460CE 0.1 -0.17046115F 0.1 -0.35674351E 0.3 -0.13267404F 0.3 -0.11042620 0.2 -0.1065720E 0.1 -0.1646460CE 0.1 -0.17046115F 0.1

<sup>a</sup> Locate the covariance matrix number on either table B-1 or B-II for a description of the events preceding TLI.

TABLE B-III.- Continued <sup>a</sup>  
Covariance Matrix

Number	LATT MATTITY	LATT QATITY	LATT MATTITY	LATT QATITY	LATT MATTITY	LATT QATITY		
75	0.501077050 0.7 -0.205774755 0.7 0.602014045 0.3 0.494650524 0.4 -0.305205242 0.2 -0.257655755 0.7	-0.60294105F 0.7 0.74730775F 0.7 0.25104425 0.4 -0.37401677 0.5 0.12431125 0.1 0.30345171F 0.2	0.435465625 0.5 -0.46707205E 0.6 0.24237611F 0.6 0.746158297 0.3 -0.67617611E 0.2 0.12551025 0.5 0.14521130E 0.6	0.11461475C 0.5 -0.12981650F 0.6 0.74614820F 0.3 -0.13456781E 0.1 0.74616852F 0.2 0.10946185E 0.1 0.12431125 0.1	-0.16521170E 0.6 0.10651702F 0.5 0.97650545 0.3 -0.97657005E 0.2 0.35499170F 0.1 -0.12191870E 0.0	0.14616738F 0.2 -0.17006050RF 0.4 0.17013220D 0.4 0.25377678F 0.1 0.14031632F 0.0 -0.12191870E 0.0	-0.24746124E 0.2 -0.25243164F 0.2 0.17013220D 0.4 -0.25377678F 0.1 -0.24746124E 0.1 -0.25243164F 0.1	
76	0.79115765 0.7 -0.67415702E 0.7 0.42544622E 0.6 -0.17614737F 0.6 -0.14521130E 0.6	0.12431125 0.7 0.46707205E 0.6 0.24237611F 0.6 0.746158297 0.3 -0.67617611E 0.2 0.12551025 0.5 0.14521130E 0.6	0.10281250E 0.7 -0.11730775F 0.6 0.27307714E 0.6 0.20433252E 0.2 -0.47240154F 0.4 -0.11730775F 0.2	0.48521655E 0.6 -0.47470542F 0.5 0.39492355E 0.3 -0.45092578E 0.2 -0.91520674E 0.1 0.17761757F 0.2	-0.112C-610F 0.4 0.4700M095F 0.2 -0.17012170F 0.2 -0.27305571E 0.1 0.14164640F 0.1 0.17761757F 0.1	-0.20048415E 0.2 -0.17622170E 0.2 0.11655891F 0.4 -0.15768676F 0.1 0.0412001F-0.2	-0.24746124E 0.2 -0.25243164F 0.2 0.17013220D 0.4 -0.25377678F 0.1 -0.24746124E 0.1 -0.25243164F 0.1	
77	0.947493701 0.6 -0.246113705 0.7 0.190036465 0.5 0.449525205 0.6	0.11461475C 0.6 -0.12981650F 0.6 0.24237611F 0.6 0.746158297 0.3 -0.67617611E 0.2 0.12551025 0.5 0.14521130E 0.6	0.10281250E 0.7 -0.11730775F 0.6 0.27307714E 0.6 0.20433252E 0.2 -0.47240154F 0.4 -0.11730775F 0.2	0.48521655E 0.6 -0.47470542F 0.5 0.39492355E 0.3 -0.45092578E 0.2 -0.91520674E 0.1 0.17761757F 0.2	-0.112C-610F 0.4 0.4700M095F 0.2 -0.17012170F 0.2 -0.27305571E 0.1 0.14164640F 0.1 0.17761757F 0.1	-0.20048415E 0.2 -0.17622170E 0.2 0.11655891F 0.4 -0.15768676F 0.1 0.0412001F-0.2	-0.24746124E 0.2 -0.25243164F 0.2 0.17013220D 0.4 -0.25377678F 0.1 -0.24746124E 0.1 -0.25243164F 0.1	
78	0.97324452F 0.6 -0.67420711E 0.7 0.90114491E 0.5 0.62865897E 0.4 -0.16606611F 0.2	0.39114617E 0.6 -0.38020505E 0.6 0.27130053E 0.6 0.1201762774F 0.5 -0.17761757F 0.5 0.127342425E 0.5 -0.11730775F 0.5	0.39114617E 0.6 -0.38020505E 0.6 0.27130053E 0.6 0.1201762774F 0.5 -0.17761757F 0.5 0.127342425E 0.5 -0.11730775F 0.5	-0.39114617E 0.6 -0.38020505E 0.6 0.1201762774F 0.5 -0.17761757F 0.5 0.127342425E 0.5 -0.11730775F 0.5	-0.15803084E 0.4 -0.17761757F 0.3 -0.1201762774F 0.3 -0.17761757F 0.3 0.127342425E 0.3 -0.11730775F 0.3	-0.15803084E 0.4 -0.17761757F 0.3 -0.1201762774F 0.3 -0.17761757F 0.3 0.127342425E 0.3 -0.11730775F 0.3	-0.37557495F 0.2 -0.17622170E 0.2 0.11655891F 0.4 -0.15768676F 0.1 0.0412001F-0.2	-0.24746124E 0.2 -0.25243164F 0.2 0.17013220D 0.4 -0.25377678F 0.1 -0.24746124E 0.1 -0.25243164F 0.1
79	0.125221125 0.7 -0.17554213 0.8 0.804746701 0.6 -0.14621170 0.5 -0.246158297 0.4	0.90647231E 0.6 -0.85745645E 0.6 0.26164636E 0.6 0.94752374F 0.6 -0.15152053E 0.5	0.90647231E 0.6 -0.85745645E 0.6 0.26164636E 0.6 0.94752374F 0.6 -0.15152053E 0.5	-0.16679111F 0.6 -0.13577221E 0.5 -0.04676416E 0.3 -0.15152053E 0.2 -0.27305571E 0.1	-0.21467911E 0.6 -0.20533721E 0.5 -0.16152053E 0.3 -0.27305571E 0.2 -0.15152053E 0.1	-0.21467911E 0.6 -0.20533721E 0.5 -0.16152053E 0.3 -0.27305571E 0.2 -0.15152053E 0.1	-0.47232167E 0.2 -0.25243164F 0.2 0.17013220D 0.4 -0.25377678F 0.1 -0.24746124E 0.1 -0.25243164F 0.1	

a Locate the covariance matrix number on either table B-1 or B-11 for a description of the events preceding T<sub>L</sub>.

TABLE B-III. - Continued

## Covariance Matrix

a Locate the covariance matrix number on either table B-1 or B-11 for a description of the events preceding T<sub>L</sub>.

TABLE B-III.- Continued a

## Covariance Matrix

Number	LAT3 MATRIX	LAT3 MATRIX	LAT3 MATRIX	LAT3 MATRIX	AL12 MATRIX
87	$\begin{matrix} 0.4415783CE & 0.7 & -0.6189961CE & 0.7 & -0.4304924E & 0.7 \\ -0.6189960CE & 0.7 & 0.80C42214E & 0.8 & -0.59235578E & 0.5 \\ -0.43C5C781E & 0.4 & -0.59235757E & 0.5 & 0.42235745E & 0.5 \\ 0.36528566E & 0.5 & -0.10572575E & 0.6 & C.439005E & 0.2 \\ -0.77890516E & 0.4 & C.13C15615E & 0.5 & -0.20264416E & 0.2 \\ 0.72097192E & 0.2 & -0.15C16123E & 0.4 & C.3C113226E & 0.5 \\ \end{matrix}$	$\begin{matrix} 0.36525959E & 0.5 & 0.7890511F & 0.4 \\ -0.10572575E & 0.5 & -0.10572575E & 0.5 \\ 0.6437303E & 0.7 & 0.34462741E & 0.3 \\ -0.20264416E & 0.2 & 0.66126164E & 0.2 \\ -0.20264416E & 0.2 & -0.66126164E & 0.2 \\ 0.34462741E & 0.3 & 0.13844061E & 0.2 \\ \end{matrix}$	$\begin{matrix} 0.7890511F & 0.4 & 0.7890511F & 0.4 \\ -0.10572575E & 0.5 & -0.10572575E & 0.5 \\ 0.20264416E & 0.2 & 0.20264416E & 0.2 \\ -0.20264416E & 0.2 & -0.20264416E & 0.2 \\ 0.20264416E & 0.2 & 0.20264416E & 0.2 \\ -0.20264416E & 0.2 & -0.20264416E & 0.2 \\ \end{matrix}$	$\begin{matrix} 0.72996387E & 0.2 \\ -0.75138562E & 0.3 \\ 0.25130697E & 0.5 \\ -0.25130697E & 0.5 \\ 0.35308090E & 0.5 \\ -0.82361317E & 0.0 \\ 0.28038789E & 0.0 \\ -0.25370179E & 0.3 \\ \end{matrix}$	
88	$\begin{matrix} 0.58652387E & 0.7 & -0.12857373E & 0.8 & 0.12666660E & 0.6 \\ -0.12857369E & 0.9 & 0.12666660E & 0.6 & C.497910C02E & 0.5 \\ -0.12666660E & 0.7 & -0.12666660E & 0.6 & -0.10414394E & 0.5 \\ 0.12666660E & 0.7 & 0.12666660E & 0.6 & C.56796387E & 0.2 \\ -0.12666660E & 0.5 & -0.12666660E & 0.5 & -0.75138562E & 0.3 \\ \end{matrix}$	$\begin{matrix} 0.12510710E & 0.5 & 0.70282756E & 0.5 \\ -0.12510710E & 0.5 & -0.12510710E & 0.5 \\ 0.92368457E & 0.6 & 0.15635205E & 0.6 \\ -0.92368457E & 0.6 & -0.15635205E & 0.6 \\ 0.75101111E & 0.3 & 0.10789691E & 0.3 \\ -0.75101111E & 0.3 & -0.10789691E & 0.3 \\ 0.65516776E & 0.3 & 0.12041882E & 0.1 \\ -0.65516776E & 0.3 & -0.12041882E & 0.1 \\ 0.28140811E & 0.2 & 0.18586631E & 0.2 \\ -0.28140811E & 0.2 & -0.18586631E & 0.2 \\ 0.82361031E & 0.0 & 0.28038789E & 0.0 \\ -0.82361031E & 0.0 & -0.28038789E & 0.0 \\ \end{matrix}$	$\begin{matrix} 0.15690751E & 0.5 \\ 0.6595751E & 0.5 \\ -0.6595751E & 0.5 \\ 0.12041882E & 0.1 \\ -0.12041882E & 0.1 \\ 0.18586631E & 0.2 \\ -0.18586631E & 0.2 \\ 0.25370179E & 0.3 \\ \end{matrix}$		
89	$\begin{matrix} 0.90655575E & 0.7 & -0.54666275E & 0.7 & 0.12510710E & 0.5 \\ -0.564662751E & 0.7 & 0.12510710E & 0.5 & 0.72993154E & 0.2 \\ 0.12530625E & 0.5 & -0.632970E & 0.6 & -0.4228223E & 0.3 \\ -0.632970E & 0.6 & 0.12530625E & 0.5 & 0.94150623E & 0.3 \\ 0.70282655E & 0.5 & -0.15635205E & 0.6 & -0.89702700E & 0.0 \\ -0.10414393E & 0.5 & 0.127474781E & 0.3 & 0.82361317E & 0.0 \\ 0.25110669E & 0.5 & -0.89702700E & 0.0 & 0.10414393E & 0.5 \\ -0.75138567E & 0.3 & C.35369090E & 0.5 & -0.28038789E & 0.0 \\ \end{matrix}$	$\begin{matrix} 0.12510710E & 0.5 & 0.70282756E & 0.5 \\ -0.12510710E & 0.5 & -0.12510710E & 0.5 \\ 0.92368457E & 0.6 & 0.15635205E & 0.6 \\ -0.92368457E & 0.6 & -0.15635205E & 0.6 \\ 0.75101111E & 0.3 & 0.10789691E & 0.3 \\ -0.75101111E & 0.3 & -0.10789691E & 0.3 \\ 0.65516776E & 0.3 & 0.12041882E & 0.1 \\ -0.65516776E & 0.3 & -0.12041882E & 0.1 \\ 0.28140811E & 0.2 & 0.18586631E & 0.2 \\ -0.28140811E & 0.2 & -0.18586631E & 0.2 \\ 0.82361031E & 0.0 & 0.25370179E & 0.3 \\ -0.82361031E & 0.0 & -0.25370179E & 0.3 \\ \end{matrix}$	$\begin{matrix} 0.4228223E & 0.2 \\ 0.143779E & 0.3 \\ 0.28442546E & 0.5 \\ -0.23510742E & 0.0 \\ 0.94201565E & -0.01 \\ 0.22041524E & -0.03 \\ \end{matrix}$		
90	$\begin{matrix} 0.42549666E & 0.7 & -0.469172.11E & 0.7 & 0.09104719E & 0.4 \\ -0.469172.11E & 0.7 & 0.469172.11E & 0.7 & 0.32937378E & 0.4 \\ 0.34681961E & 0.8 & -0.10021686E & 0.8 & -0.48241671E & 0.5 \\ -0.10021686E & 0.8 & 0.34681961E & 0.8 & 0.77123370E & 0.4 \\ 0.398223H1E & 0.7 & 0.10445978E & 0.3 & 0.33915414E & 0.2 \\ -0.10445978E & 0.3 & C.10446600E & 0.3 & 0.26085600E & 0.3 \\ -0.42241671E & 0.5 & 0.10446600E & 0.3 & 0.56668842E & 0.2 \\ -0.73144497E & 0.4 & -0.33915414E & 0.2 & 0.12632565E & 0.2 \\ 0.77123370E & 0.4 & 0.56668841E & 0.2 & -0.94201565E & -0.01 \\ -0.73144497E & 0.4 & -0.12632565E & 0.2 & 0.22041524E & -0.03 \\ 0.22041524E & 0.2 & C.28464254E & 0.5 & 0.22041524E & -0.03 \\ \end{matrix}$	$\begin{matrix} 0.32937378E & 0.4 \\ 0.143779E & 0.3 \\ 0.28442546E & 0.5 \\ -0.23510742E & 0.0 \\ 0.94201565E & -0.01 \\ 0.22041524E & -0.03 \\ \end{matrix}$			
91	$\begin{matrix} 0.45105565CE & 0.7 & -0.51538602E & 0.7 & -0.70449956E & 0.4 \\ -0.51538602E & 0.7 & 0.44722616E & 0.8 & C.1655A8594E & 0.4 \\ 0.1655A8594E & 0.8 & -0.1655A8594E & 0.4 & -0.1334277E & 0.5 \\ 0.42549666E & 0.4 & 0.42549666E & 0.7 & -0.14527103E & 0.2 \\ -0.14527103E & 0.7 & C.14527344E & 0.2 & 0.18653442E & 0.2 \\ -0.14527344E & 0.2 & 0.29570572E & 0.3 & 0.67651805E & 0.2 \\ 0.14527344E & 0.2 & -0.62661807E & 0.2 & 0.13798075E & 0.2 \\ -0.9130916E & 0.4 & -0.19653320E & 0.2 & 0.13433773E & 0.3 \\ 0.21735603E & 0.3 & C.31052418E & 0.5 & -0.95673320E & 0.3 \\ \end{matrix}$	$\begin{matrix} 0.70449956E & 0.4 \\ 0.21735376E & 0.3 \\ 0.31052418E & 0.5 \\ -0.95673320E & 0.3 \\ 0.22280413E & 0.3 \\ \end{matrix}$			
92	$\begin{matrix} 0.92669955E & 0.7 & -0.11231657E & 0.9 & C.407C4429E & 0.5 \\ -0.11231657E & 0.9 & C.13539273E & 0.9 & -0.117C9481E & 0.6 \\ 0.407C4429E & 0.5 & -0.67228803E & 0.6 & 0.7427917E & 0.3 \\ -0.67228803E & 0.6 & C.89424267E & 0.7 & 0.13387030E & 0.3 \\ 0.7427917E & 0.7 & C.65241773E & 0.3 & -0.13433223E & 0.3 \\ -0.7427917E & 0.3 & -0.13433773E & 0.3 & 0.2980108CE & 0.2 \\ -0.16244923E & 0.5 & C.1387193F & 0.5 & -0.96735615E & 0.2 \\ 0.26063210E & 0.3 & G.63773552E & 0.5 & 0.45760120E & 0.3 \\ \end{matrix}$	$\begin{matrix} 0.74477807E & 0.5 \\ 0.26063210E & 0.3 \\ 0.63773552E & 0.5 \\ -0.13433223E & 0.3 \\ 0.6698032F & 0.2 \\ 0.45760120E & 0.3 \\ \end{matrix}$			

a Locate the covariance matrix number on either table B-1 or B-11  
 for a description of the events preceding Tl.

TABLE B-III.—Continued a  
Covariance Matrix

a Locate the covariance matrix number on either table B-1 or B-11 for a description of the events preceding TLI.

TABLE B-III.- Continued <sup>a</sup>

## Covariance Matrix

Number	LAT3 MATRIX	C7	-0.463224441E 06	-0.52384375E 03	0.11548763E 05	-0.26869453E 04	-0.29951782E 01
99	0.15484033E C6	0.13655514E 06	-0.17058027E 04	-0.34547299E 04	0.60383902E 03	-0.12426025E 02	
	-0.463224440E C6	0.12255529E 05	0.15856354E 07	-0.21722421E 01	-0.6698596E 01	0.11372461E 05	
	-0.52383594E C3	-C17C58C47E 04	0.15856354E 07	-0.21722421E 02	-0.20043397E 02	-0.12345791E -01	
	0.11468784E C5	-0.345473C0E 04	-0.6658749E 01	0.86163577E 02	0.46629508E 01	-0.4882264E -01	
	-0.26869453E C4	C18C35C0E 03	-0.6658749E 01	-0.20043398E 02	0.46629508E 01	-0.4882264E -01	
	-0.29951782E C1	-C12426117E 02	0.11372421E 05	-0.12345791E -01	-0.48823178E -01	0.81674325E 02	
	LAT3 MATRIX	C7	-0.12244666CE 07	-0.13848125E 04	0.30509978E 05	-0.71000232E 04	-0.79161377E 01
100	0.40522270E C7	0.26639294E 06	-0.42290156E 04	-0.91287389E 04	0.21244380E 04	-0.32835154E 02	
	-0.122446660E 07	0.42012132E 04	0.57431641E 07	-0.57431641E 01	-0.17112768E 02	0.30043505E 05	
	-0.13847969E 04	-C45C09C00CE 04	0.57430420E 01	0.22714968E 03	-0.52937732E 02	-0.32634735E -01	
	0.30509978E C5	-C1287394CE 04	-0.57430420E 02	-0.52937733E 02	0.2318968E 02	-0.12904477E 00	
	-0.71CC0330E C4	C2124438CE 04	-0.17112707E 02	-0.32634735E 01	-0.12904549E 00	0.21562936E 03	
	-0.79157715E 01	-0.22855663E 02	0.30C435C3E 05	-0.32634735E 01	-0.12904549E 00	0.21562936E 03	
	AT3 MATRIX	C7	-0.14406232E 07	-0.16253437E 04	C.35894466E 05	-0.83532347E 04	-0.93125986E 01
101	C.48145C70E C7	0.4108058E 06	-0.53050469E 07	-0.10740011E 05	0.24994541E 04	-0.38632019E 02	
	-0.14406232E 07	0.5205C469E 04	0.67576904E 05	-0.67576904E 01	0.20840324E 02	0.3345595E 05	
	-0.16233753E C4	-0.5205C469E 05	-0.67576904E 01	0.26763187E 03	-0.62278671E 02	-0.383949228E -01	
	0.25564466E C5	-0.1C140010E 05	-0.20840454E 02	-0.62278871E 02	0.14493069E 02	-0.15182734E 00	
	-0.8252346E C4	0.245954543E 04	-0.35345555E 05	-0.38394928E -01	-0.15182710E 00	0.25366913E 03	
	-0.93134766E C1	-0.36632263E 02	0.35345555E 05	-0.71653366E -01	-0.28332281E 00	0.47323913E 03	
	AT3 MATRIX	C7	-0.26682275E 07	-0.30406875E 04	0.6674368E 05	-0.15586862E 05	-0.17379639E 02
102	0.89646699E C7	0.80466485E 06	-0.20040460E 05	-0.20040460E 04	0.46640906E 04	-0.72086304E 02	
	-0.26682375E 07	-0.58993737E 04	0.92235467E 07	-0.12610107E 02	-0.38891906E 02	0.65949898E 03	
	-0.304066815E 04	-0.58993962E 04	0.92235467E 07	-0.49929582E 03	0.16119703E 03	-0.7165366E -01	
	0.66574368E 05	-0.20040460E 05	-0.1261032E 02	-0.11619703E 03	0.21042231E 02	-0.28332138E 00	
	-0.15586861E C5	C46640907E 04	-0.38891845E 02	-0.71653366E -01	-0.28332281E 00	0.47323913E 03	
	-0.17775639E C2	-0.72086121E 02	0.65949898E 05	-0.15586862E 05	-0.77371150E -02	0.20713467E 01	
	LAT3 MATRIX	C7	0.70216246E 07	-0.23757422E 03	-0.73424071E 04	-0.1696620E 04	-0.10605293E 02
103	0.20242650E C7	0.12355988E 09	0.51527944E 09	-0.14074551E 06	0.1022471E 04	-0.52302059E 02	
	0.10218251E C7	0.12255529E 05	0.75683014E 06	-0.64697510E 02	0.37679749E 01	0.12161294E 05	
	-0.23757613E C3	0.54692250E 05	0.21626180E 07	-0.65022368E 02	0.18647946E 02	-0.34994680E 03	
	-0.112544613E C5	0.54692250E 05	0.21626180E 07	-0.19846670E 03	-0.13919092E 02	0.2582632E -01	
	0.1538835E C4	-0.15576903E 06	-0.65C22887E 02	-0.13919000E 02	0.33344555E 01	-0.16072113E -02	
	-0.15515614E C1	-0.12161293E 05	0.19647095E 02	-0.25825500E -01	-0.16053515E -02	0.78616319E -01	
	-0.10414124E C2	-0.19455557E 02	-0.34954524E 03	-0.25825500E -01	-0.16053515E -02	0.78616319E -01	

<sup>a</sup> Locate the covariance matrix number on either table B-I or B-II for a description of the events preceding T<sub>1</sub>.

TABLE B-III. - Continued<sup>a</sup>  
Covariance Matrix

Number	LAT3 MATRIX	LAT3 MATRIX	LAT3 MATRIX	LAT3 MATRIX	LAT3 MATRIX	LAT3 MATRIX	LAT3 MATRIX	
105	0.395C1828E C7 0.19503664E C8 0.61760258E C4 -0.22193701E C5 -0.18588550E C4 -0.15128174E C2	0.199C3659E C8 0.80857242E C9 0.352C7790E C6 -0.93349020E 06 0.62425E84E 05 -0.17427735E 03	0.61765547E 04 0.39207677E 06 0.72986766E 06 -0.45826686E 03 0.42425E84E 05 -0.17427735E 02	-0.22193705E 05 -0.93349020E 06 -0.45826686E 03 0.42425E84E 02 -0.17427735E 04	-0.18998578E 04 0.63425497E 05 0.34214233E 02 -0.74132240E 02 0.84546356E 01 -0.26994865E 02	-0.15115345E 02 -0.17428613E 03 0.12377986E 04 0.18953157E 00 0.84546356E 01 -0.26994865E 02	-0.15115345E 02 -0.17428613E 03 0.12377986E 04 0.18953157E 00 0.84546356E 01 -0.26994865E 02	-0.15115345E 02 -0.17428613E 03 0.12377986E 04 0.18953157E 00 0.84546356E 01 -0.26994865E 02
106	0.25442698E 07 0.50179467E 07 -0.94548150E 04 -0.80147543E C4 -0.20537241E C4 -0.16057739E C1	0.5C17552CE 07 0.69856083E C9 0.42015830E 06 0.10776226E 07 0.9171871.6E 05 -0.11423735E 02	0.42015838E 06 0.2166C6992E 07 0.42015830E 06 -0.49987110E 03 0.56693359E 02 -0.12935126E 04	-0.94958828E 04 0.14485182E 07 0.73634444E 06 -0.10776226E 03 0.56694406E 02 -0.35820C15E 03	-0.80147549E 04 -0.33442811E 07 -0.1688983E 04 -0.10802200E 03 0.12093680E 02 -0.13858795E 00	-0.20837215E 04 0.27182224E 06 0.14058447E 03 -0.10802159E 03 0.12093680E 02 -0.10905743E -01	-0.16038494E 01 -0.11423123E 03 0.12401193E 04 0.13856545E 00 -0.109026282E -01 0.81401739E 01	-0.16038494E 01 -0.11423123E 03 0.12401193E 04 0.13856545E 00 -0.109026282E -01 0.81401739E 01
107	0.61712159E C7 0.60351687E C8 0.26344750E C5 -0.92466933E C5 0.94739331E C3 -0.22533594E 02	0.60391704E 08 0.268015829E 10 0.14485339E 07 -0.33442811E 07 0.27184221E 06 -0.45570313E 03	0.263645238E 05 0.14485182E 07 0.73634444E 06 -0.10776226E 03 0.56694406E 02 -0.35820C15E 03	-0.692464953E 05 -0.33442811E 07 -0.1688983E 04 -0.38822423E 04 -0.14059718E 03 -0.2166C6992E 03	-0.94739478E 03 0.27182224E 06 0.14058447E 03 -0.31649382E 03 0.303021193E 02 -0.29731350E 01	-0.22951721E 02 -0.45565564E 03 0.12401193E 04 -0.51726479E 00 -0.29731350E 01 0.21581237E 01	-0.22951721E 02 -0.45565564E 03 0.12401193E 04 -0.51726479E 00 -0.29731350E 01 0.21581237E 01	
108	0.10525322E C7 -0.545410559E 07 -0.60337683E 08 -0.17362844E 06 -0.58720938E 04 -0.14716001E 04	0.54410559E 07 0.26033202H 08 0.17675413E 07 0.26450333E 05 0.40746016E 05 0.12407078E 04	0.26033202H 07 0.13473631E 07 0.26450333E 05 0.40746016E 03 0.12407078E 02 0.42490258E 01	0.58720938E 04 -0.89332027E 05 -0.2045341E 04 -0.925246221E 02 -0.13444600E 02 -0.40746016E 01	-0.14716001E 04 0.12809109E 05 0.40746019E 03 -0.13444600E 02 0.25509996E 01 -0.40746016E 00	-0.55987759E 03 -0.42490258E 03 -0.43446006E 02 -0.90233915E 00 -0.18685595E 01 -0.29701233E -01	-0.55987759E 03 -0.42490258E 03 -0.43446006E 02 -0.90233915E 00 -0.18685595E 01 -0.29701233E -01	
109	0.87324287E C6 0.15441508E C7 -0.17582219E 06 -0.17218595E 04 -0.67792564E 03 -0.63134705E 02	0.1521421438E C7 0.15955236E C9 0.44392362E C7 0.13473631E 07 -0.51266232E 04 -0.23059409E 03 0.340142034E 03	0.1521421438E C7 0.15955236E C9 0.44392362E C7 0.13473631E 07 -0.51266232E 04 -0.23059409E 03 0.340142034E 03	-0.17582248E 05 -0.11780845E 06 -0.51706064E 05 -0.131313704E 04 -0.73227963E 03 -0.13187147E 02 0.80723211E 02	-0.17218524E 04 -0.11780845E 05 -0.51706064E 04 -0.131313704E 03 -0.73227963E 02 -0.13187147E 01 0.80723211E 00	-0.57792249E 03 -0.12809109E 04 -0.25359940E 03 -0.131313704E 02 -0.73227963E 01 -0.13187147E 00 0.80723211E 00	-0.57792249E 03 -0.12809109E 04 -0.25359940E 03 -0.131313704E 02 -0.73227963E 01 -0.13187147E 00 0.80723211E 00	
110	0.32319601E C6 -0.43654861E C7 -0.28910675E 04 -0.62162157E 04 -0.68887634E 03 -0.81113373E 02	-0.49654711E 07 -0.79075205E 04 -0.24711852E 05 -0.32221180E 05 -0.80887634E 05 -0.14057314E 02	-0.289106605E 04 -0.34224908E 05 -0.70329102E 02 -0.25091248E 01 -0.13187147E 02 -0.17934761E 01	-0.60152183E 04 -0.96591182E 05 -0.34214233E 02 -0.74132240E 02 -0.13187145E 02 -0.15793152E 01	-0.68887592E 03 -0.25091248E 02 -0.13187147E 01 -0.17934761E 01 -0.13187145E 00 -0.19910970E 00	-0.63134906E 02 -0.15793152E 03 -0.34214233E 02 -0.74132240E 02 -0.13187145E 01 -0.19910970E 00		

a Locate the covariance matrix number on either table B-1 or B-II  
for a description of the events preceding TII.

TABLE B-III.- Continued<sup>a</sup>

## Covariance Matrix

Number	A13 MATRIX	LAT3 MATRIX	LAT3 MATRIX	LAT3 MATRIX	LAT3 MATRIX	
111	$\begin{matrix} 0.1055692E-07 & -0.1145719E-08 & 0.1281241E-06 & 0.13694139E-05 & -0.14010123E-04 & 0.66310471E-02 \\ -0.1145672E-05 & 0.12272167E-09 & -0.11502524E-07 & -0.152641912E-08 & 0.129208824E-05 & -0.171271100E-03 \\ C.12312445E-06 & -0.11303525E-07 & 0.183039310E-06 & 0.1653091dE-04 & -0.15186478E-03 & 0.2055328E-02 \\ C.13324134E-05 & -0.11242412E-05 & 0.16330910E-04 & -0.147500E-03 & -0.14222539E-02 & 0.66345305E-00 \\ -0.20510117E-04 & 0.152524952E-05 & -0.12186430E-03 & -0.21422539E-02 & 0.1777875E-01 & -0.12832370E-00 \\ C.6631193E-02 & -0.11211191E-03 & 0.20555656E-02 & 0.180345190E-00 & -0.12832284E-00 & 0.20406056E-01 \end{matrix}$	$\begin{matrix} 0.00921174E-05 & -0.24957864E-07 & 0.15608992E-05 & 0.33058867E-04 & -0.28201593E-03 & -0.25347144E-02 \\ -0.29278631E-07 & 0.12195887E-09 & -0.68372172E-06 & -0.13631144E-06 & 0.11426599E-05 & 0.10136326E-04 \\ 0.1508387E-05 & -0.60372174E-06 & 0.12991534E-05 & 0.76382880E-05 & -0.63962707E-02 & 0.56123199E-01 \\ C.330588869E-04 & -0.13041173E-06 & 0.70382917E-03 & 0.15236591E-03 & -0.12739069E-02 & -0.11316902E-01 \\ -0.28271566E-03 & 0.11435071E-05 & -0.3902427E-02 & -0.12739070E-02 & 0.1823710E-01 & 0.94852683E-01 \\ C.25347137E-02 & 0.11430313E-04 & 0.26120415E-01 & -0.11316912E-01 & 0.94852149E-01 & 0.51722214E-01 \end{matrix}$	$\begin{matrix} 0.1257299E-08 & -0.71458910E-07 & 0.31980000E-04 & 0.94816764E-05 & -0.21552052E-05 & -0.70680176E-02 \\ -0.71458903E-07 & 0.3567931E-08 & -0.11021814E-06 & -0.66540067E-05 & 0.12742513E-05 & 0.72955078E-02 \\ 0.31980000E-04 & -0.11021784E-06 & 0.12506557E-08 & 0.65414951E-02 & -0.74955200E-02 & 0.89278942E-05 \\ 0.94816764E-05 & -0.66540069E-05 & 0.6541062E-02 & 0.72125251E-03 & -0.16278172E-03 & -0.49325562E-00 \\ -0.21552052E-05 & 0.12742513E-05 & -0.74955688E-02 & -0.16278171E-03 & 0.42259104E-02 & -0.38409996E-00 \\ -0.70680176E-02 & 0.72954530E-02 & 0.89278941E-05 & -0.49325562E-00 & -0.38410187E-00 & 0.63989883E-03 \end{matrix}$	$\begin{matrix} 0.12950240E-08 & -0.76241794E-07 & -0.86753750E-04 & 0.98360980E-05 & -0.22263615E-05 & -0.75277832E-02 \\ -0.76241795E-07 & 0.45592820E-08 & -0.83998750E-04 & -0.77149408E-05 & 0.14071212E-05 & 0.14550952E-03 \\ -0.86755625E-04 & -0.8397812E-04 & 0.12932233E-08 & -0.536646728E-02 & -0.60019836E-02 & 0.92272612E-05 \\ 0.98340979E-05 & -0.79149405E-05 & -0.53645996E-02 & 0.75909744E-03 & -0.16247044E-03 & -0.58813858E-00 \\ -0.22263616E-05 & 0.14071213E-05 & -0.60019897E-02 & -0.16247085E-03 & 0.4381987E-02 & -0.3872229E-00 \\ -0.75277832E-02 & 0.14550879E-02 & 0.92272613E-05 & -0.58814240E-00 & -0.38722134E-00 & 0.6613045E-03 \end{matrix}$	$\begin{matrix} 0.18175402E-08 & -0.13868884E-08 & 0.33085250E-05 & 0.14990412E-06 & -0.31618364E-05 & 0.85930176E-02 \\ -0.13868883E-08 & 0.1630288E-09 & -0.68296103E-06 & -0.19060723E-06 & 0.2391800E-05 & -0.24348667E-04 \\ 0.33885125E-05 & -0.68296087E-06 & 0.1675147E-08 & 0.6437744E-03 & -0.1765149E-03 & 0.12908759E-06 \\ 0.14090412E-06 & -0.19060724E-05 & 0.69437695E-03 & 0.11477084E-04 & -0.24835374E-03 & 0.22433204E-01 \\ -0.31618363E-05 & 0.29391801E-05 & -0.17765284E-03 & -0.24835374E-03 & 0.6063659E-02 & -0.91611671E-00 \\ 0.85328711E-02 & -0.2348682E-04 & 0.12908759E-06 & 0.22433167E-01 & -0.91610909E-00 & 0.92547232E-03 \end{matrix}$	$\begin{matrix} 0.71081039E-06 & -0.359622290E-07 & 0.72128886E-04 & 0.63985564E-04 & -0.97334186E-03 & -0.47733658E-02 \\ C. -0.35962283E-07 & 0.34612703E-08 & -0.971466274E-05 & -0.400815221E-05 & 0.65844081E-04 & 0.16812902E-03 \\ 0.7228555E-04 & -0.97146031E-05 & 0.32849218E-06 & 0.820666765E-02 & -0.21600868E-02 & 0.22337506E-04 \\ 0.63985558E-04 & -0.40081521E-05 & 0.820666765E-02 & 0.62199251E-02 & -0.93916985E-01 & -0.39863598E-00 \\ -0.97334206E-03 & 0.65844083E-04 & -0.23600903E-02 & -0.93916986E-01 & 0.65844056E-01 & -0.10011107E-01 \\ -0.4733826E-02 & 0.16812927E-03 & 0.22137505E-04 & -0.39863539E-00 & -0.10011107E-01 & 0.15251238E-02 \end{matrix}$
114						
115						
116						

<sup>a</sup>Locate the covariance matrix number on either table B-I or B-II for a description of the events preceding TII.

TABLE B-III.- Concluded<sup>a</sup>

## Covariance Matrix

Number	LAT3 MATRIX															
	0.48139877E 06	-0.39528138E 07	-0.45226582E 04	0.68912912E 04	-0.97934898E 03	-0.51543915E 02										
	-0.39528141E 07	0.444494172E 08	0.511197651E 04	-0.52383710E 05	0.77019725E 04	0.24394702E 03										
117	-0.45228593E 04	0.51198750E 04	0.36663409E 06	-0.3622912E 02	-0.69044266E 01	0.2223292E 01										
	0.68912909E 04	-0.52383710E 05	-0.36442293E 02	0.77448072E 02	-0.10821747E 02	-0.49027514E 00										
	-0.97934922E 03	0.77019728E 04	-0.69043274E 01	-0.10821747E 02	0.66572667E 01	-0.30618908E 03										
	-0.51543640E 02	0.24394702E 03	0.22232329E 04	-0.49027586E 00	-0.30633807E-03	0.15239966E 02										
	LAT3 MATRIX															
	0.89057070E 06	-0.86965182E 07	0.39735682E 05	0.12066164E 05	-0.16322434E 04	0.11936532E 03										
	-0.86965175E 07	0.13475506E 09	-0.66391370E 06	-0.15205335E 06	0.20418562E 05	-0.2296183E 04										
118	0.39735625E 05	-0.66391350E 06	0.32996367E 06	0.71864238E 03	-0.10282044E 03	0.2211670E 01										
	0.12066164E 05	-0.15205335E 06	0.71864235E 03	0.18737365E 03	-0.24842567E 02	0.23811847E 01										
	-0.16322420E 04	0.20418562E 05	-0.10282184E 03	-0.24842566E 02	0.84426391E 01	-0.37101498E 00										
	0.11936432E 03	-0.22961816E 04	0.22211671E 04	0.23811846E 01	-0.37101376E 00	0.15271519E 02										

<sup>a</sup> Locate the covariance matrix number on either table B-1 or B-11  
for a description of the events preceding TLL.

APPENDIX C

TRANSLUNAR PHASE PROCEDURE

## APPENDIX C

## TRANSLUNAR PHASE PROCEDURE

The  $\Delta V$  cost of the first midcourse correction is computed from the following formulation taken directly from reference 8. Given the particular position and velocity of a vehicle, the  $\Delta V$  required for the midcourse can be computed. The procedure for computing midcourse  $\Delta V$  is based on a simple guidance scheme and, for the present, on the assumption that the post injection orbit is well known compared to the expected deviation of the actual orbit from the nominal.

The deviations in position and velocity at midcourse correction time ( $t_M$ ) and at some target time  $t$  are approximately related by the following linear expression

$$\begin{bmatrix} \delta X \\ \delta \dot{X} \end{bmatrix}_t = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} \delta X \\ \delta \dot{X} \end{bmatrix}_{t_M}$$

The deviation in position is just

$$\delta X_t = A\delta X_M + B\delta \dot{X}_M$$

where  $X$  is a three element position vector and  $A$  and  $B$  are  $3 \times 3$  matrices. The guidance law assumed is simply that a change in velocity is made at  $t_M$  to achieve the proper position at a target time  $t$ . That is,

$$\delta X_t = A\delta X_M + B(\delta \dot{X}_M + \Delta V), \text{ where } \Delta V \text{ is the amount to be added to make}$$

$$\delta X_t = 0. \text{ This expression can be written for } \Delta V.$$

$$\begin{aligned} B(\delta \dot{X}_M + \Delta V) &= \delta X_t - A\delta X_M \\ \Delta V &= B^{-1}(\delta X_t - A\delta X_M) - \delta \dot{X}_M \end{aligned}$$

Since  $\Delta V$  is taken to make  $\delta X_t = 0$ , this becomes

$$\Delta V = -B^{-1}A\delta X_M - \delta \dot{X}_M$$

or

$$\Delta V = -\left[B^{-1}A, I\right] \delta \begin{pmatrix} X_M \\ \dot{X}_M \end{pmatrix}$$

The expected value of  $\Delta V$  then becomes

$$\begin{aligned} E(\Delta V, \Delta V^T) &= E \left[ (B^{-1} A, I) \delta \begin{pmatrix} x_M \\ \dot{x}_M \end{pmatrix}^{\delta}(x_M^T, \dot{x}_M^T) \begin{pmatrix} [B^{-1} A]^T \\ I \end{pmatrix} \right] \\ &= (B^{-1} A, I) E \left[ \delta \begin{pmatrix} x_M \\ \dot{x}_M \end{pmatrix}^{\delta}(x_M^T, \dot{x}_M^T) \right] \begin{pmatrix} [B^{-1} A]^T \\ I \end{pmatrix} = L P_M L^T \end{aligned}$$

where  $L = (B^{-1} A, I)$  and  $P_M$  is the covariance matrix of the position and velocity at  $t_M$ . The target time will be the time of lunar sphere of influence. What is desired is not the expected value of  $\Delta V$  but the scalar  $\Delta v$ . This is given by

$$\Delta v = \left[ \frac{2}{\pi} (\sigma_{\Delta V_x}^2 + \sigma_{\Delta V_y}^2 + \sigma_{\Delta V_z}^2) \right]^{\frac{1}{2}}$$

The  $\frac{2}{\pi}$  factor is the first term in a series expression developed by Breakwell (ref. 9).

The target time used for this study was 51.5 hours after the TLI maneuver. No drag or venting was considered outside earth orbit. The covariance matrix of position and velocity at the time of the midcourse correction is generated by propagating the covariance at the end of TLI with two-body partials. The ground-computed estimate of position and velocity was assumed to be the actual vector at the time of the first MCC.

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